

# Technologies for Seismic Retrofitting and Strengthening of Earthen and Masonry Structures: Assessment and Application

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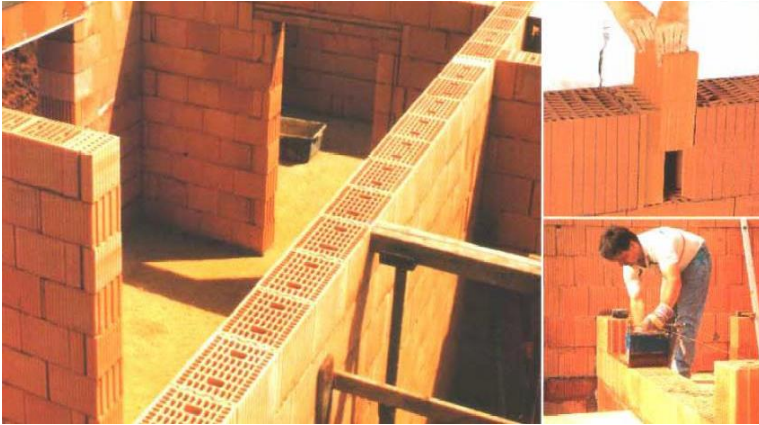


# Introduction

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## What is masonry?



**A material with visible internal structure and low tensile strength:**  
Rubble masonry is not much different from unreinforced concrete or earth

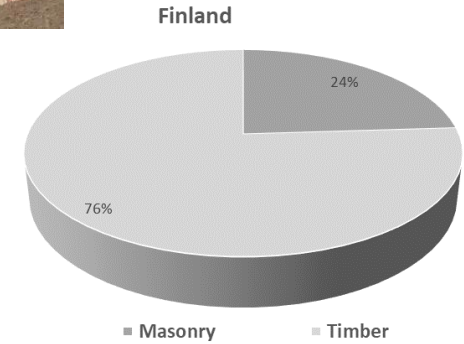
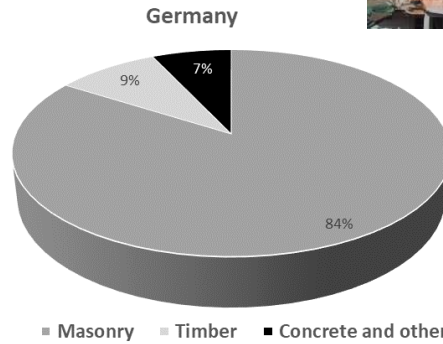
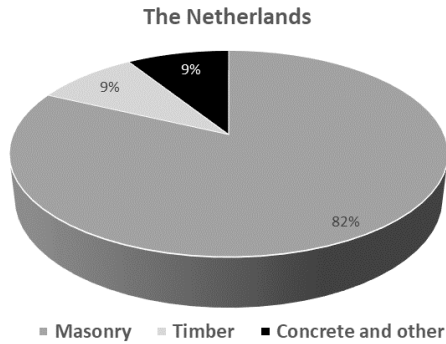
## Existing built heritage

Global Building Inventory of twenty-two moderate to high seismicity, developed and developing, countries indicates, in which unreinforced masonry (URM) accounts for **more than half of the built heritage** (Jaiswal and Wald 2008)

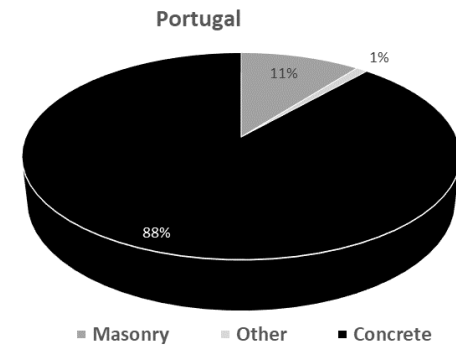
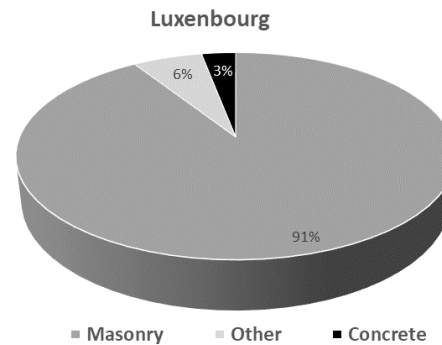
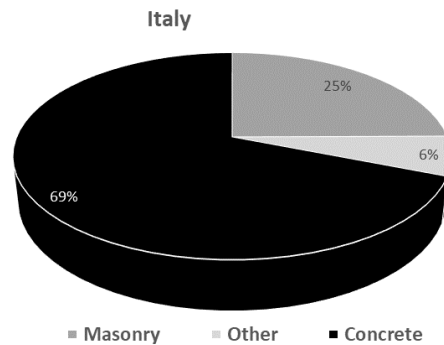
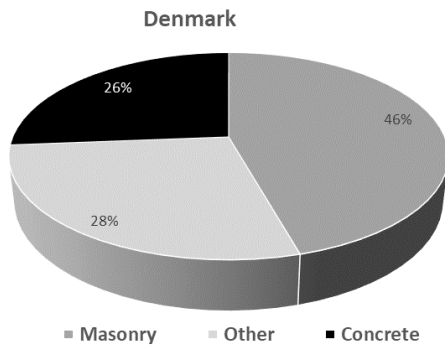
| Country       | Year | URM as % of inventory |
|---------------|------|-----------------------|
| Australia     | 2000 | 52.9                  |
| El Salvador   | 1990 | 48.0                  |
| Indonesia     | 2001 | 60.0                  |
| Iran          | 2005 | 56.7                  |
| Italy         | 2006 | 62.2                  |
| Mexico        | 2000 | 75.7                  |
| New Zealand   | 1998 | 7.0                   |
| Pakistan      | 1998 | 93.0                  |
| Peru          | 2007 | 73.2                  |
| Philippines   | 2000 | 30.8                  |
| Turkey        | 2002 | 47.1                  |
| United States | 2002 | 15.0                  |

**(Frankie, Gencturk, and Elnashai 2013)**

# Modern buildings



## Residential market (Pompeu Santos 2007)



## Building structures (Sousa and Carvalho 2007)



Cusco, 1950



Ancash, 1970

Pisco, 2007

Misca, 2014



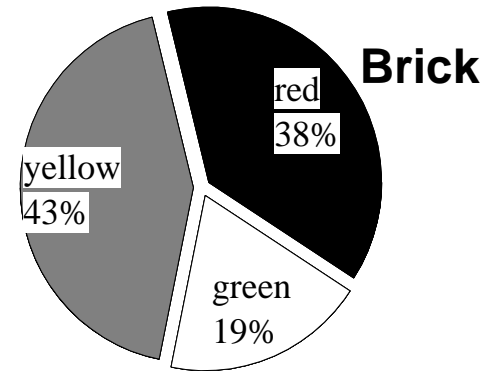
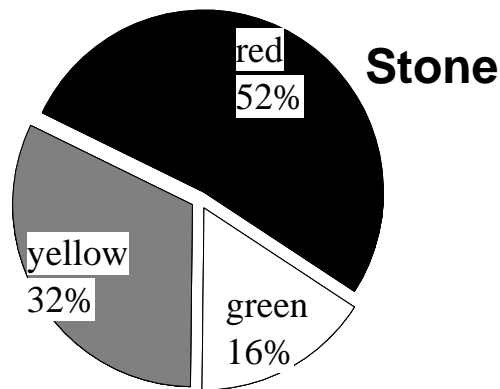
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## Arequipa, Peru



## Example of churches in New Zealand (Earthquakes 2010-11)

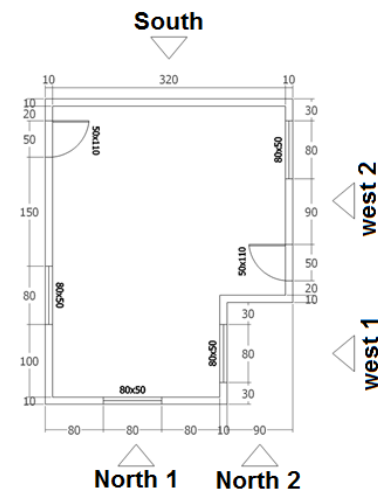
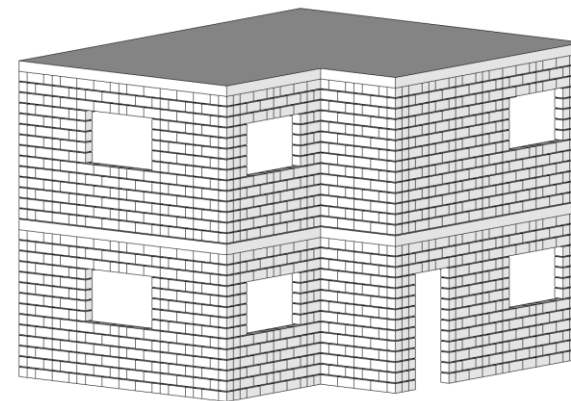
- ❑ Red: unsafe building with access forbidden
- ❑ Yellow: safety compromised but urgent access allowed
- ❑ Green: no restrictions





## Modern masonry as good as other building technology

- ❑ Worst case scenario in masonry: embedded ring beam + unfilled vertical joints
- ❑ Light damage up to the design earthquake in Lisbon (rock)
- ❑ Ductile damage for 2.5x the design earthquake in Lisbon (rock),  $q = 2.5$



# Blind test prediction

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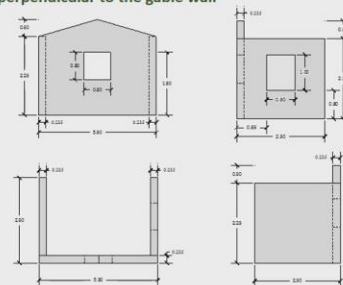


## Existing Masonry Buildings: Without rigid diaphragm

- ❑ Recent benchmark test
- ❑ 25 international masonry experts
- ❑ 18 blind predictions
- ❑ 2 masonry types

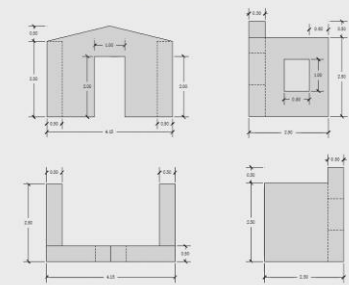
### Structure with clay-unit masonry and English bond

- Unreinforced gable wall and return walls on both ends
- Perforated bricks and cement-based mortar
- An opening in one of the returning walls, resulting in an asymmetry, and consequently, inducing torsional movements
- Thickness of the walls equal to 0.235 m
- Unidirectional seismic action perpendicular to the gable wall



### Structure with stone masonry units

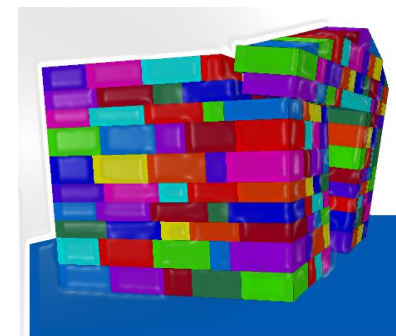
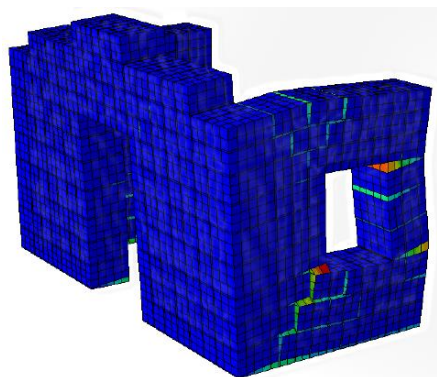
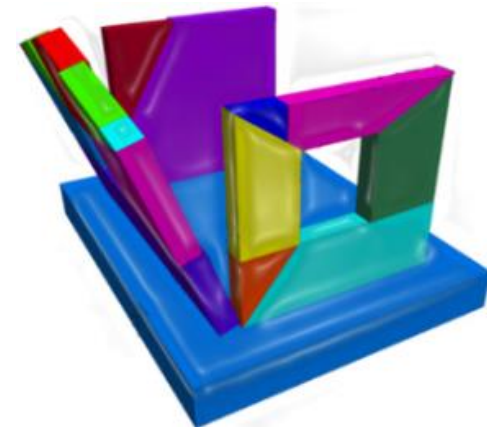
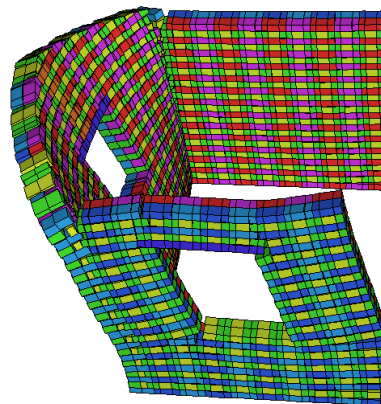
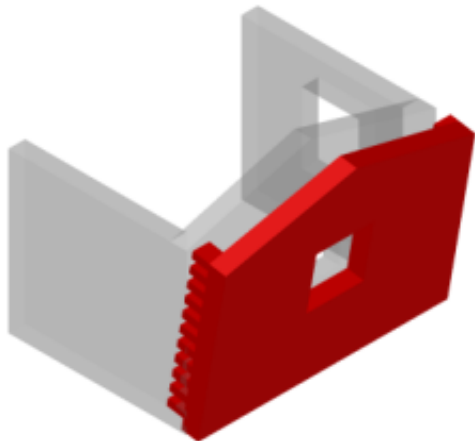
- Unreinforced gable wall and return walls on both ends
- Stone units and lime-based mortar
- An opening in one of the returning walls, resulting in an asymmetry, and consequently, inducing torsional movements
- Thickness of the walls equal to 0.50 m
- Unidirectional seismic action perpendicular to the gable wall



## Data given & approaches adopted

- ❑ Geometry
- ❑ Material properties (specific mass, Young's modulus, tensile and compressive strength)
- ❑ Normalized accelerogram envelopes of the seismic action applied at the base, and the corresponding response spectra
  
- ❑ Modelling approaches adopted:
  - rigid macro-blocks (23 models)
  - finite element modeling (7 macro-models, 3 micro-models)
  - discrete element method (3 meso-models)
  
- ❑ Type of structural analysis:
  - ❑ Limit analysis based on the kinematic approach;
  - ❑ Static non-linear analysis (pushover), usually mass (a few first mode) proportional
  - ❑ Non-linear dynamic analysis with time integration, with artificial accelerograms applied at the base of structures generated by the experts

## Examples of models adopted by experts



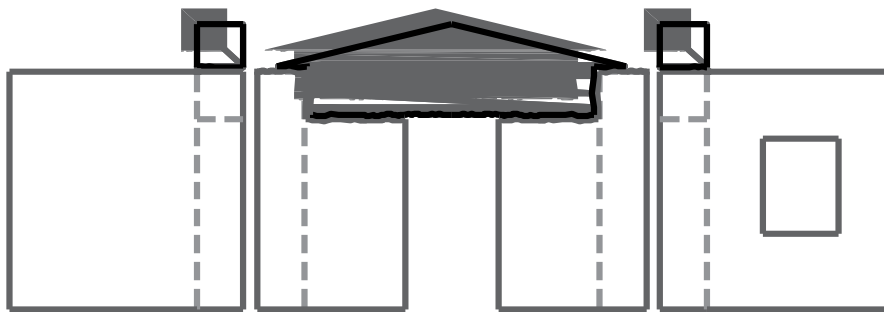
Macro-blocks

FEM

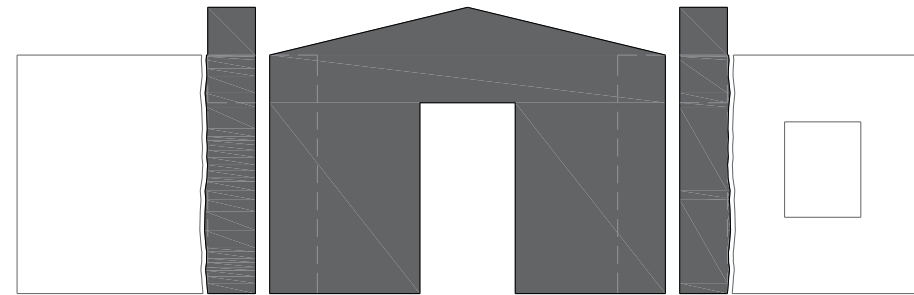
DEM

## Stone building: 13 idealized collapse mechanism proposed

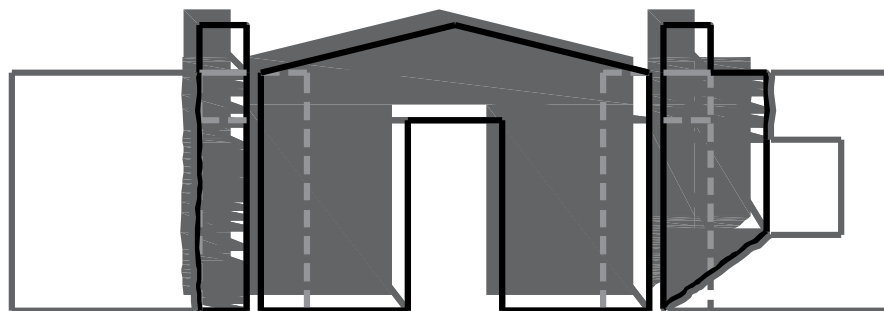
- ❑ Estimated PGA at collapse ranged from 0.22-2.50 g (COV=63%)
- ❑ Average estimated PGA of 0.91 g (Experimental equal to 1.07 g)
- ❑ Large variance due to incorrect prediction of collapse mechanism. For mechanisms similar to test, prediction range was 0.53-1.42 g (COV= 31%)



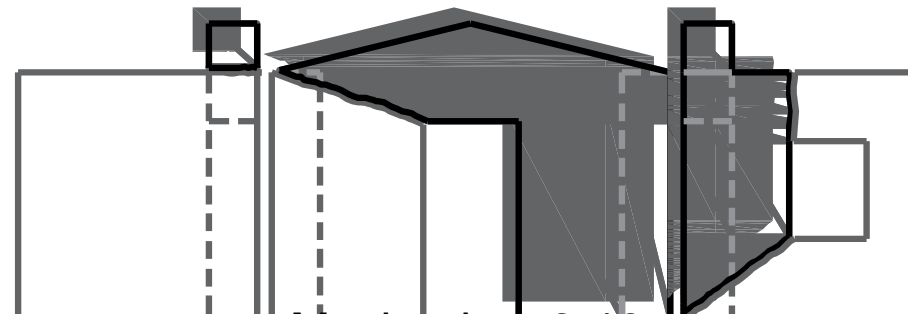
Mechanisms 1-4



Mechanism 5



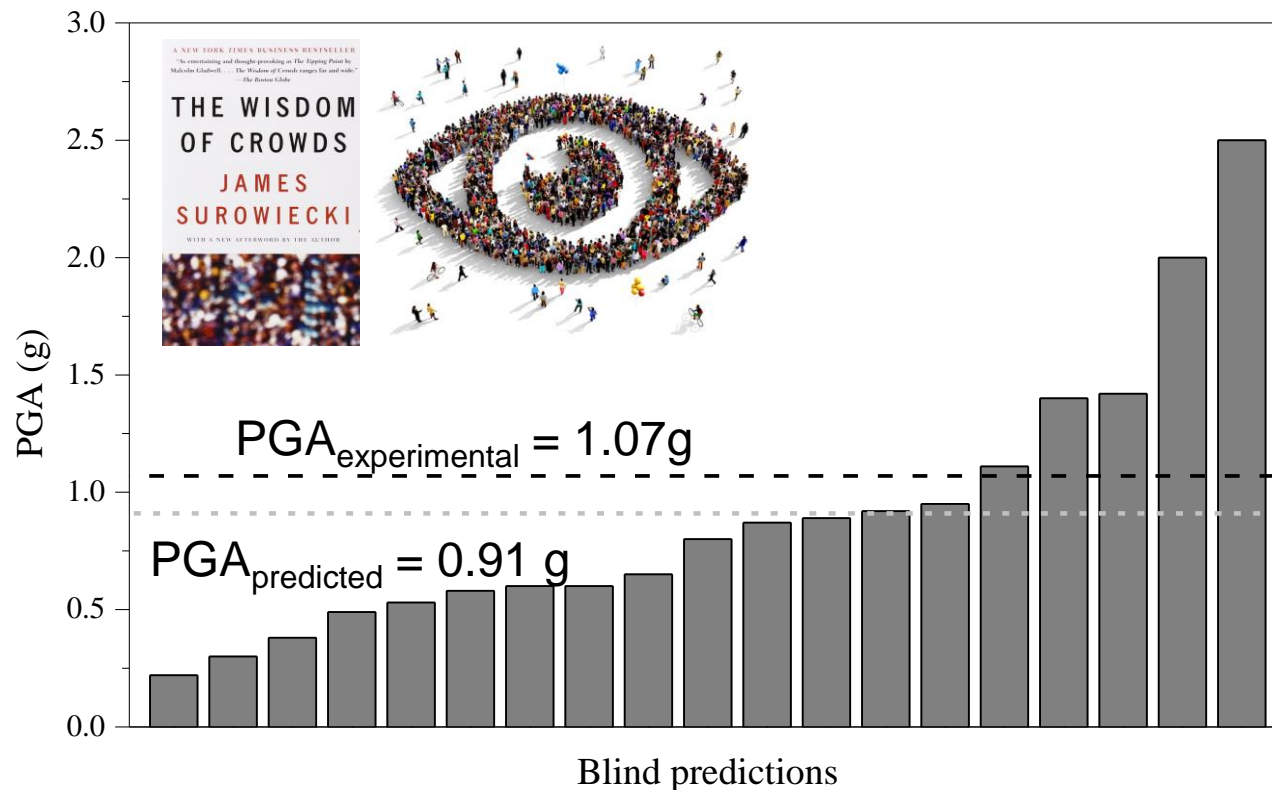
Mechanism 6-7



Mechanism 9-13

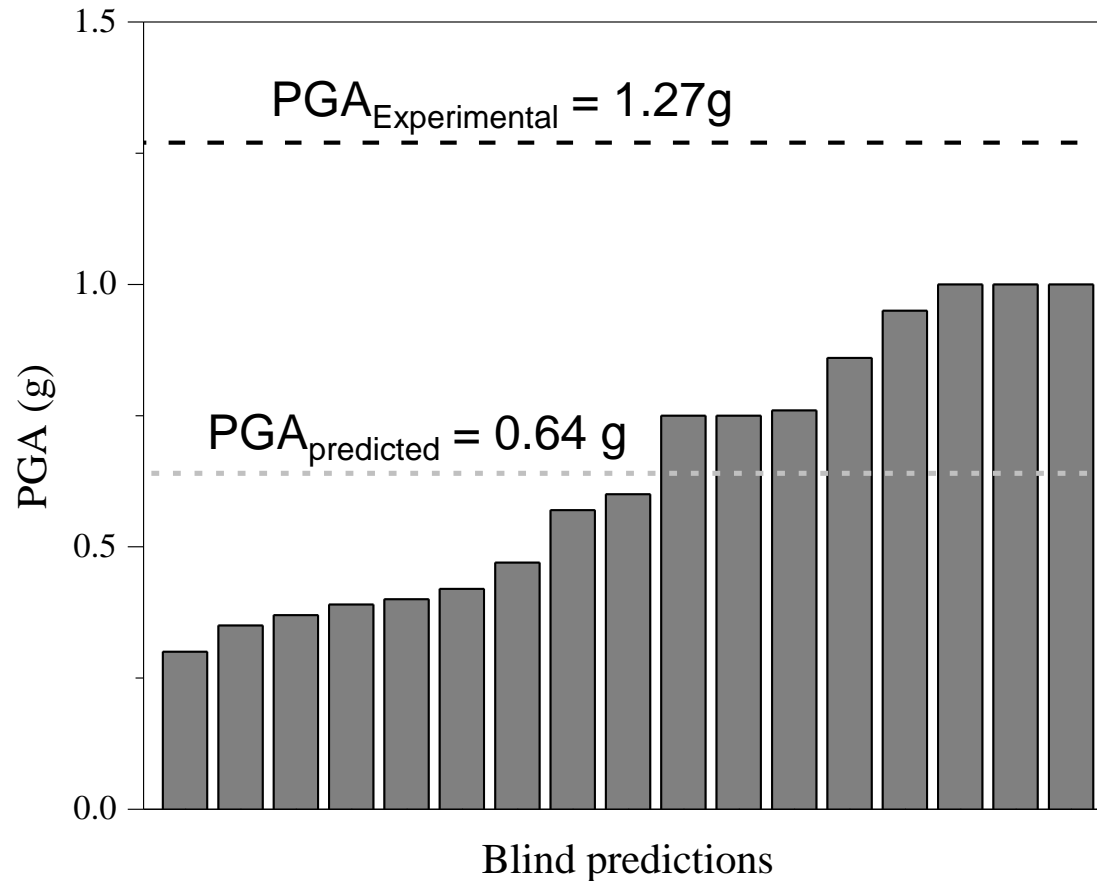
## Stone building: 13 idealized collapse mechanism proposed (II)

- ❑ Average error between test and predicted PGA for good mech. was 28%
- ❑ 80% presented a predicted PGA lower than or equal to test
- ❑ Within good mech., two results presented collapse displacement at top (0.16 and 0.25 m). Test provided 0.22 m (about half of the wall thickness).



## Brick building

- ❑ 17 predictions. Estimated PGA at collapse: 0.30-1.00 g (COV=39%)
- ❑ Experimental result (1.27 g). Average PGA of predictions: 0.64 g. All predictions lower than experimental results
- ❑ Problems: slenderness of the structure, torsional effects, material properties?





## It seems that...

- We can make assessments on the safe side
- Too much scatter in predictions is found
- Masonry out-of-plane failure assessment remains a research challenge

# Engineering applications to earthen structures

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## Earthen structures

- About 2 billion people (almost 50% of the population in developing countries)



## Historic earthen structures

- ❑ Significant portion of the built heritage worldwide



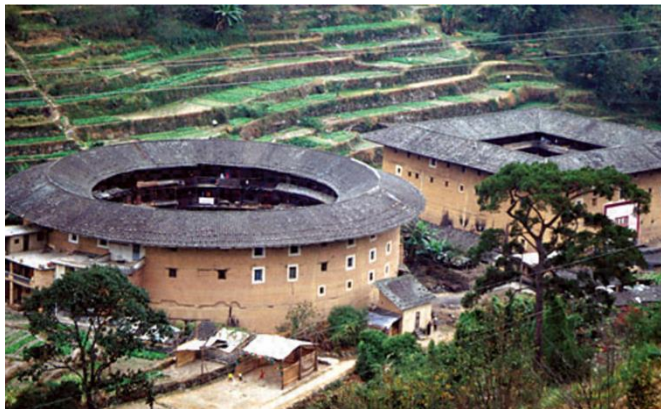
Houses of Tiébélé (Burkina Faso)



Arg-e-Bam (Iran)



Mosque of Djenné (Mali)



Hakka dwellings (China)



Kasbah Taourirt (Marocco)

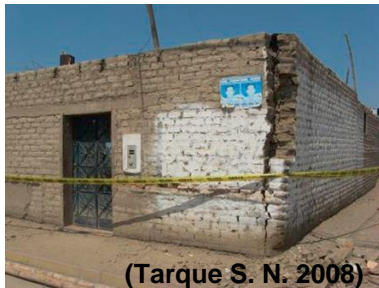
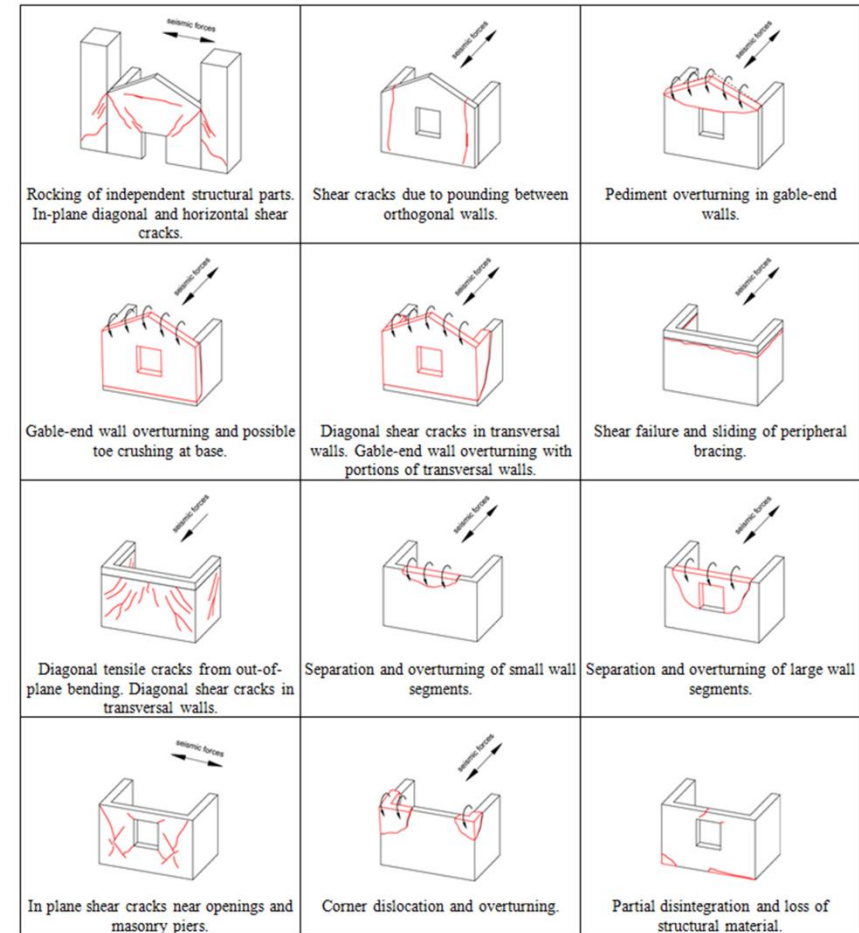
## Historic earthen structures

- ❑ Building techniques with intangible historical value, wide material availability and low-cost construction

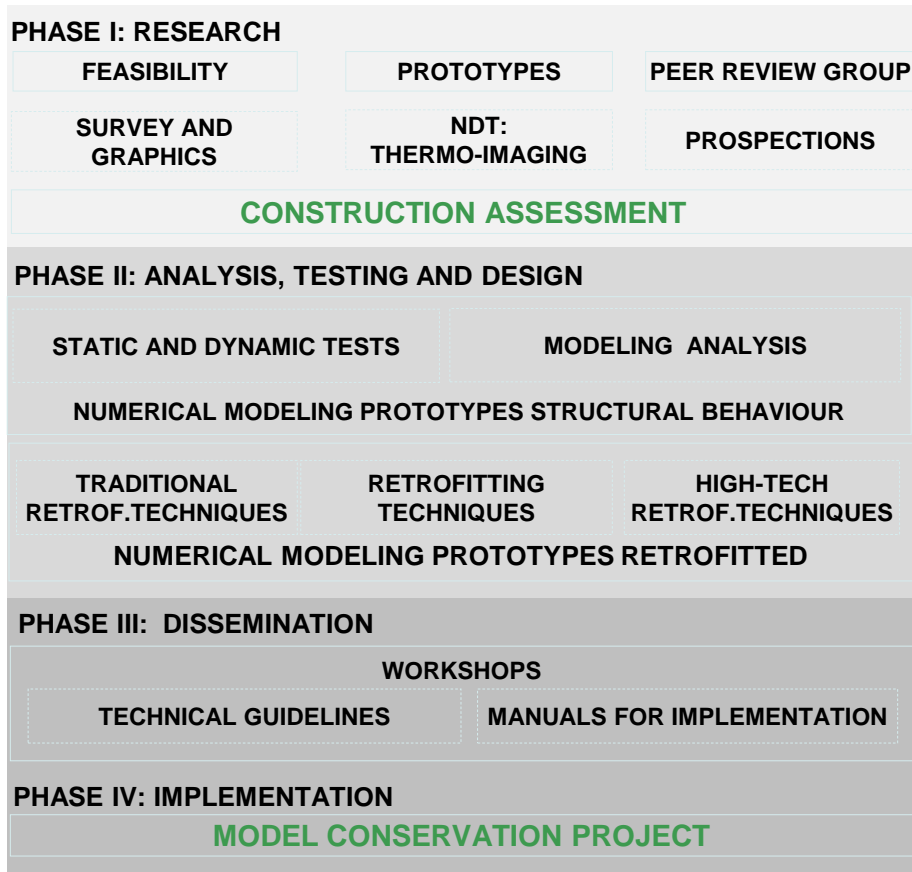


# Seismic vulnerability

- ❑ Poor mechanical properties
- ❑ Lack of lateral confinement
- ❑ Lack of maintenance



# Seismic Retrofitting Project (SRP), after GSAP Seismic Stabilization of Historic Structures (1990–96)



## Prototype buildings



Church of Kuño Tambo



Casa Arones



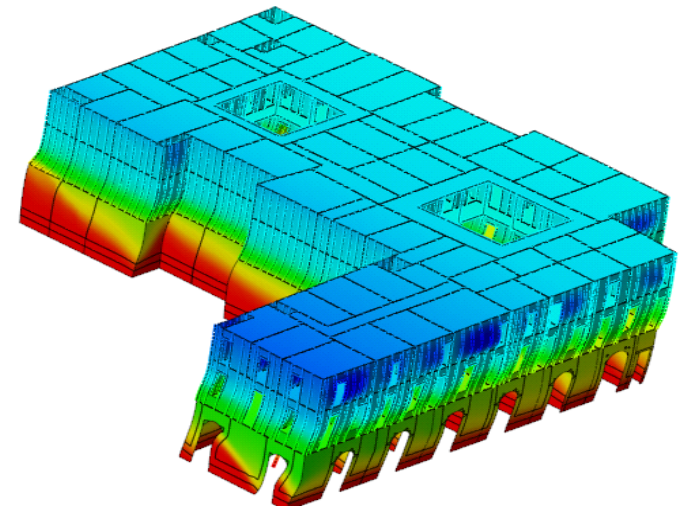
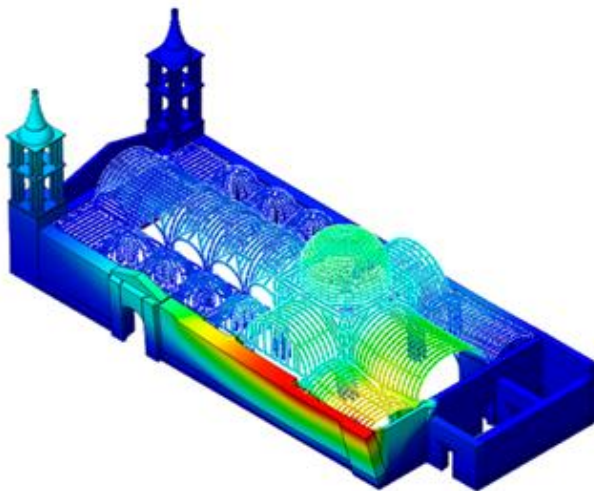
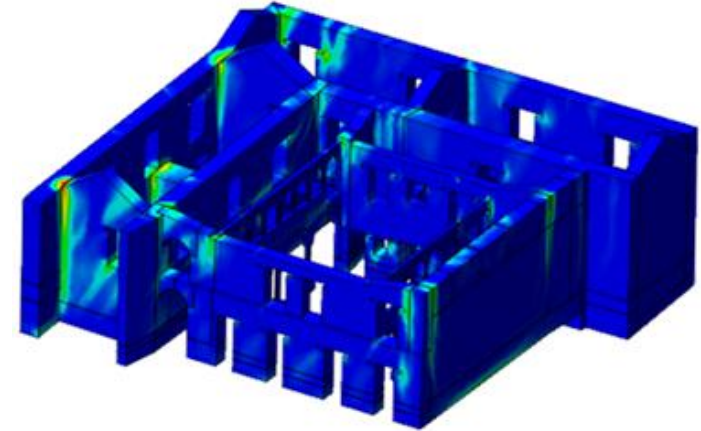
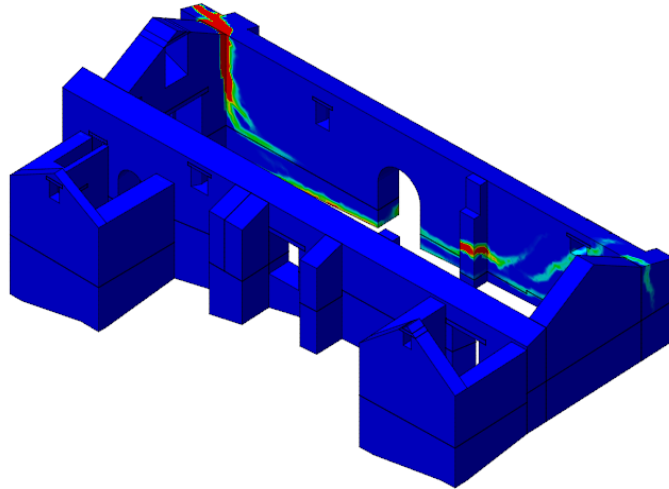
Ica Cathedral



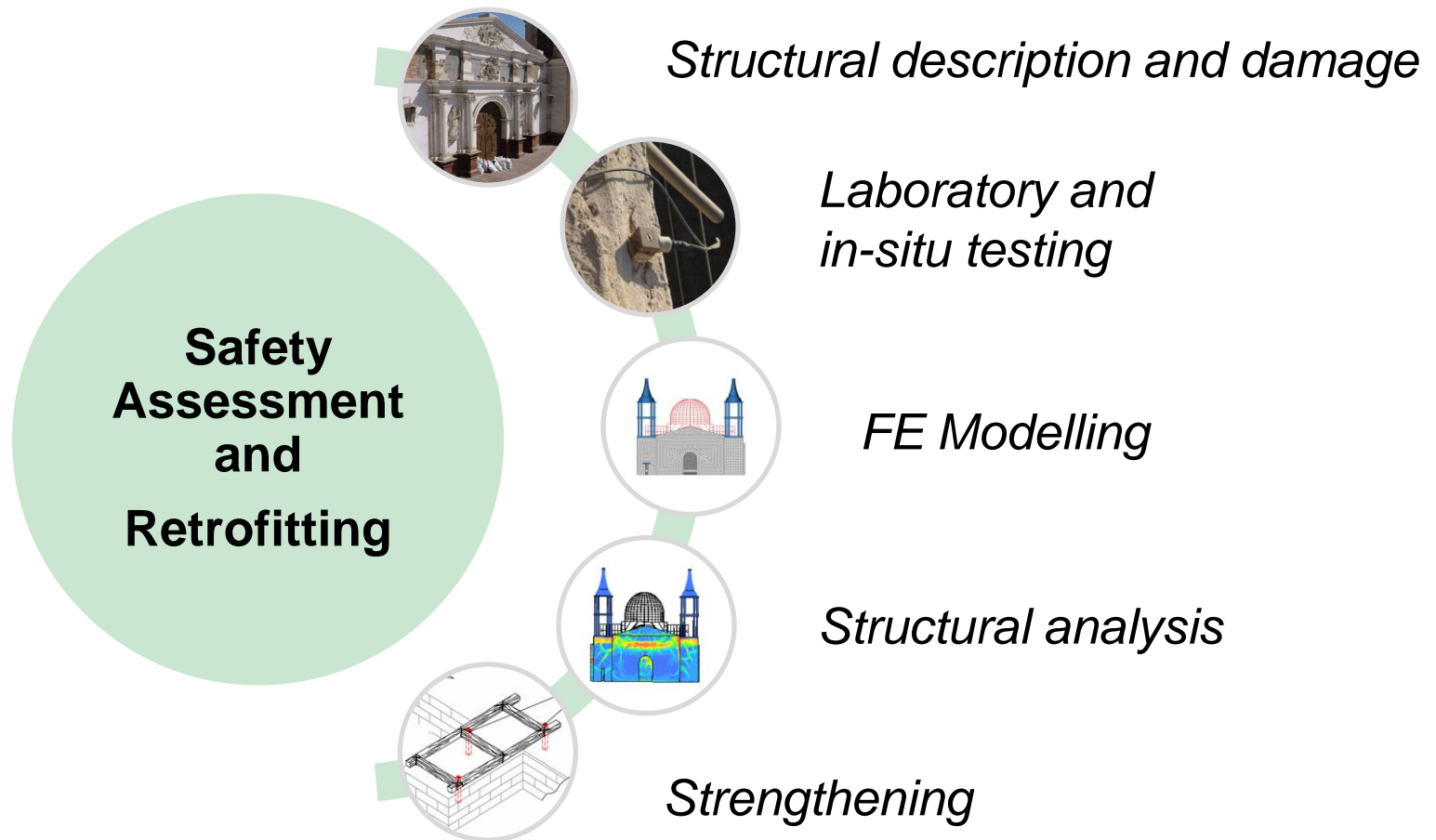
Hotel El Comercio



## Our Role



# Methodology



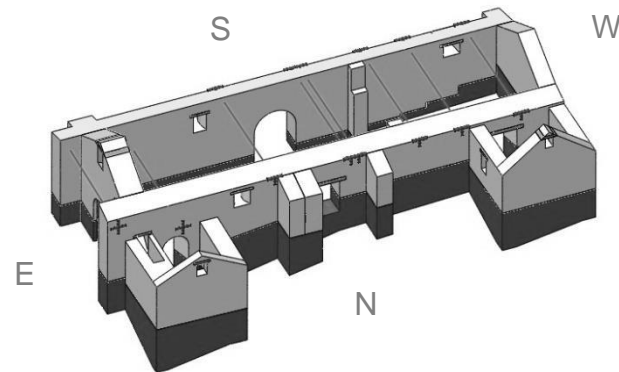
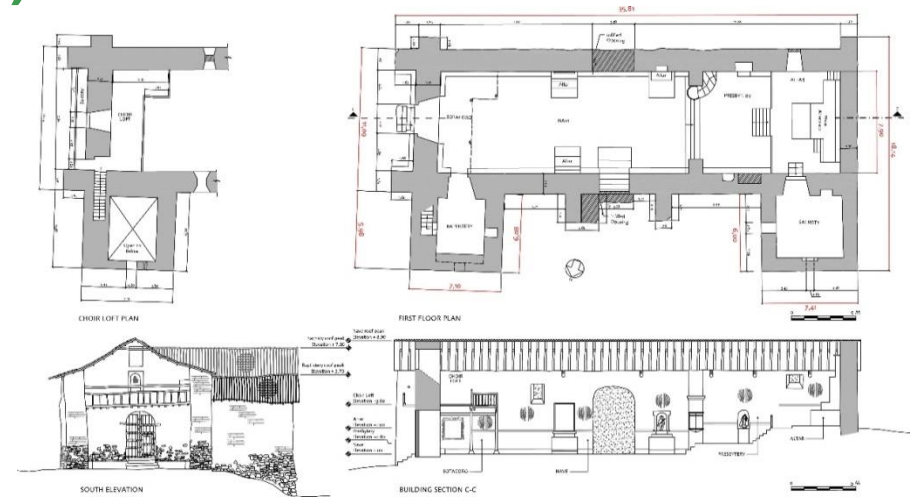
# Structural description and damage

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## Church of Kuño Tambo (KT)

- ❑ Built in **17<sup>th</sup> century**
- ❑ **Structure**
  - Single nave with a sacristy and a baptistery
  - Adobe walls with rubble stone base course
  - Buttresses
  - Single gable timber roof
  - Timber ties and wall plates



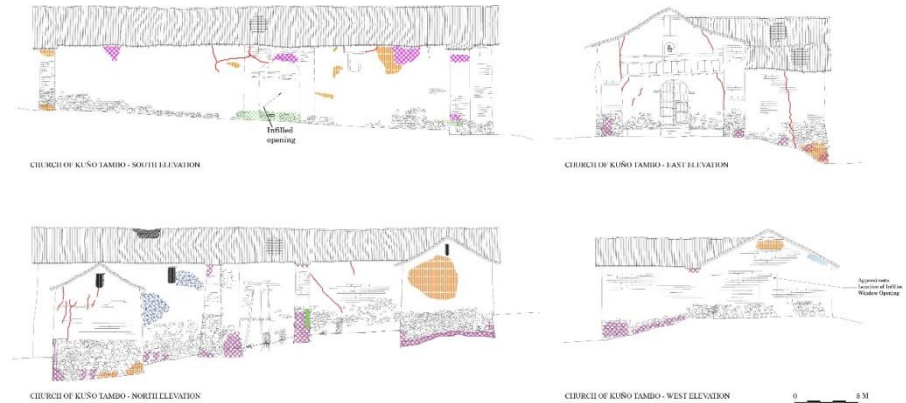
# Church of Kuño Tambo (KT)

## Damage

- Vertical cracks
- Loss of material
- Deterioration

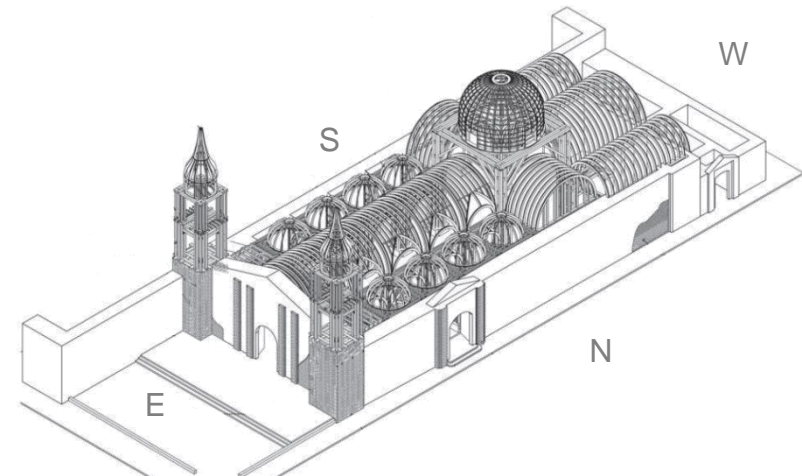
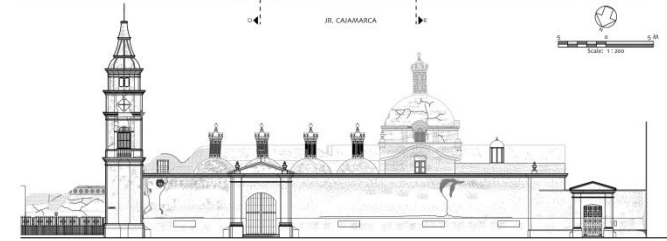
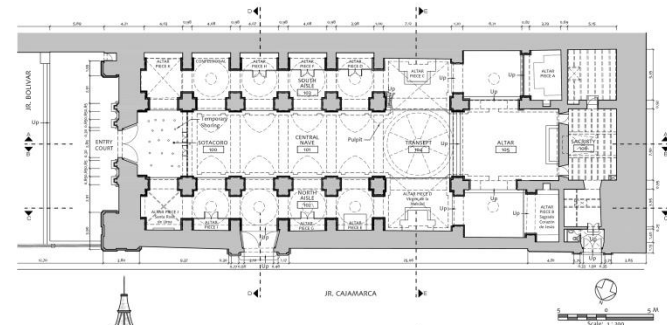
## Diagnosis

- Earthquakes
- Settlements
- Lack of maintenance



## Ica Cathedral (IC)

- ❑ Built in **18<sup>th</sup> century**, national monument since 1982
- ❑ **Structure**
  - External masonry envelope (rubble stone, fired brick, rubble stone)
  - Internal timber frame (*quincha* technique)



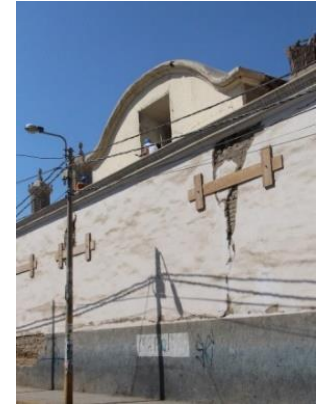
## Ica Cathedral (IC)

### ❑ Damage

- Collapse of the roof system
- Vertical cracks
- Loss of material
- Deterioration

### ❑ Diagnosis

- Earthquakes in 2007 (MW 7.9-8.0) and in 2009 (MW 5.8)
- Lack of maintenance



# Laboratory and in-situ testing

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## Laboratory testing

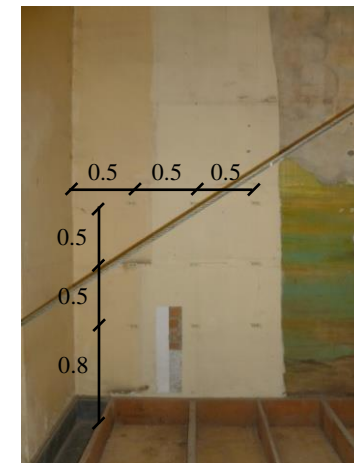
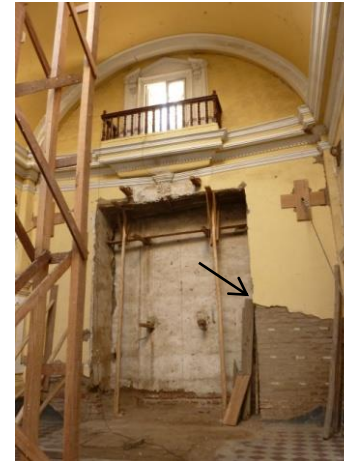
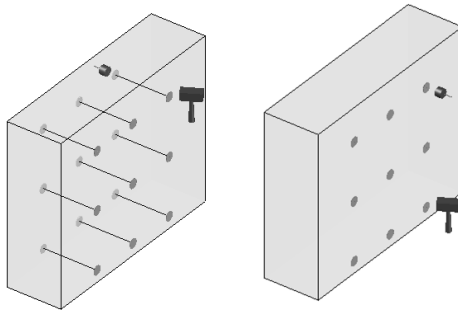
- ❑ **Material properties**
- ❑ **Behaviour of traditional structural systems**
- ❑ **Tests**
  - Adobe, brick, timber and lime mortar
  - Adobe and brick masonry
  - *Quincha* panels and timber connections
  - Traditional strengthening techniques



Laboratory tests performed by PUCP

## Sonic tests

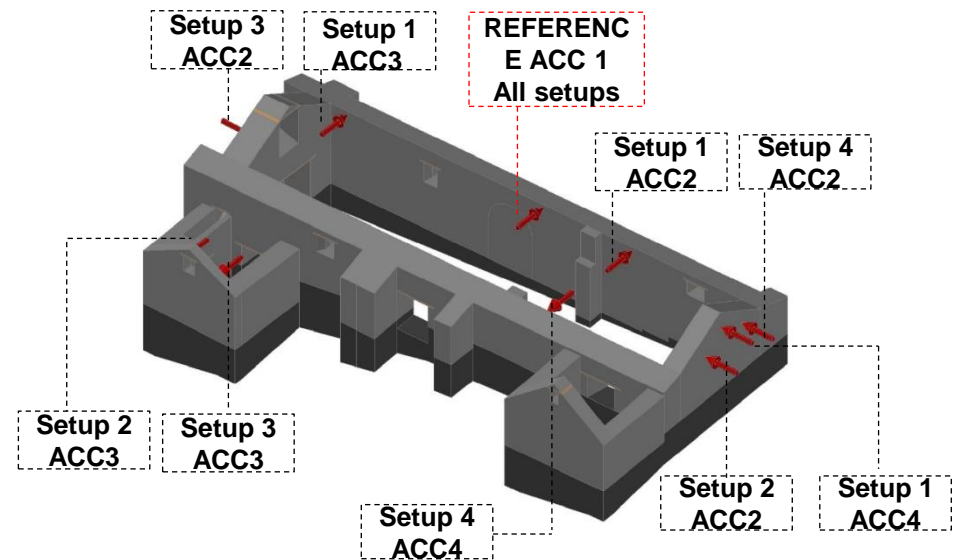
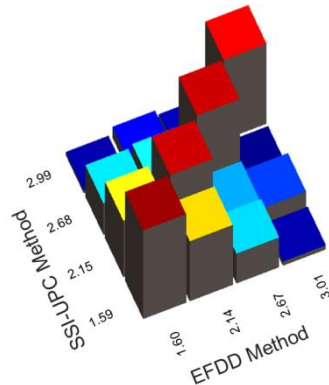
- ❑ Morphology
- ❑ Mechanical properties
- ❑ Tests
  - Direct tests
  - Indirect tests



Sonic tests performed by UMinho

## Dynamic identification tests

- ❑ Dynamic characteristics
- ❑ Calibration of the numerical models
- ❑ Test
  - Output-only (or ambient vibration) technique during service conditions

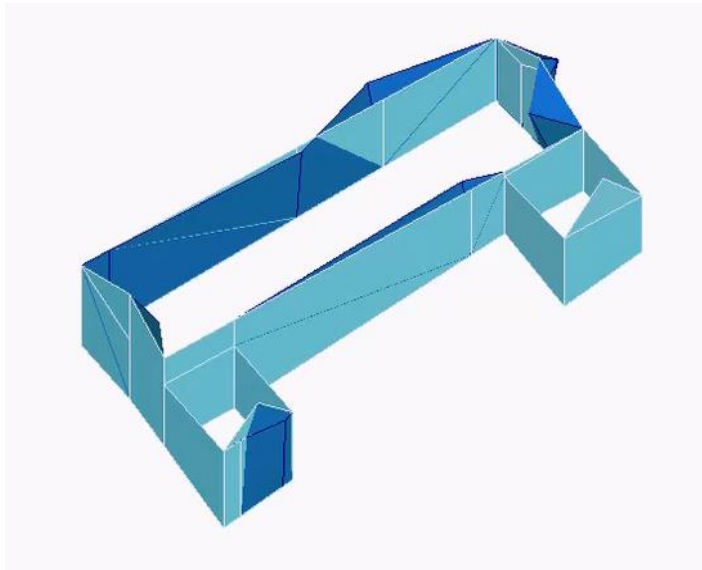


Dynamic identification tests performed by UMinho

## Dynamic identification tests

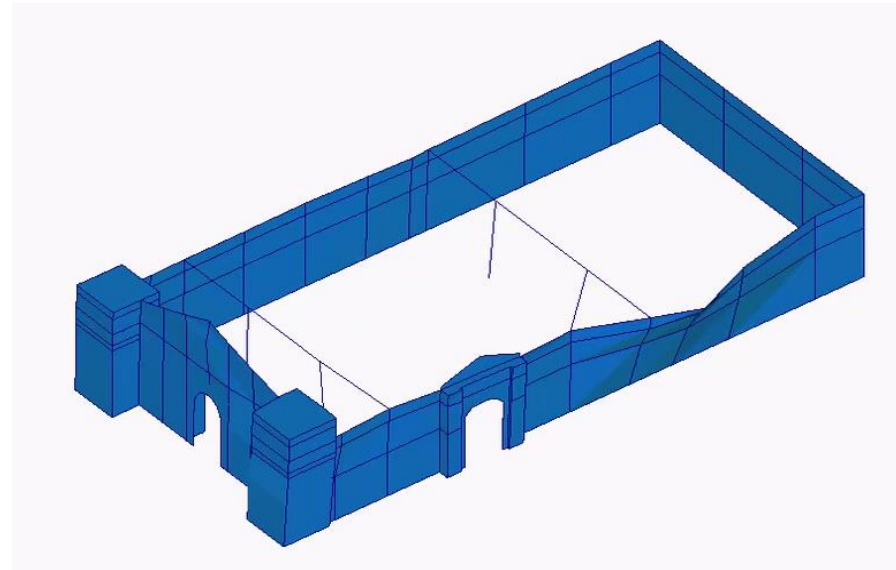
### ☐ Church of Kuño Tambo

- Poor connection at the corners
- Ineffectiveness of the existing tie beams



### ☐ Ica Cathedral

- Poor connection between the masonry and timber substructures



# Finite element modelling and structural analysis

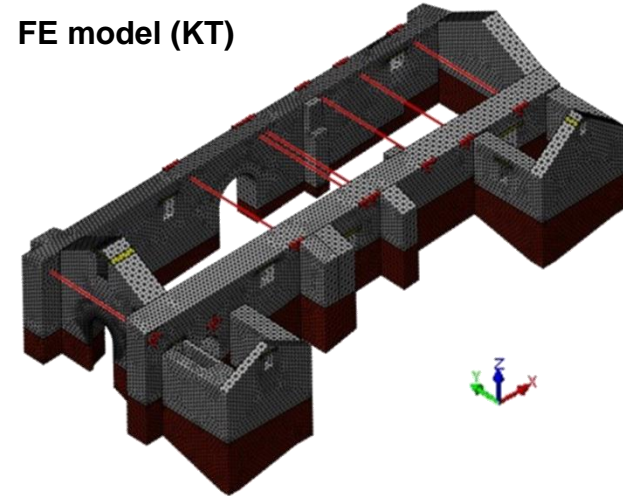
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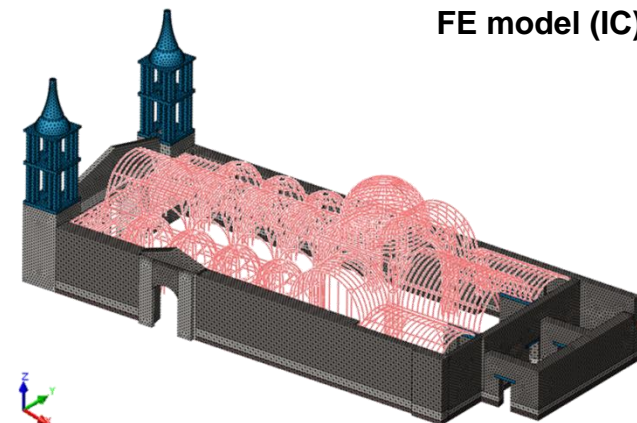
## Finite Element (FE) modelling

- ❑ 3D macro-modeling FE approach
- ❑ Partial and global models
- ❑ Models created in Midas FX+ for DIANA software

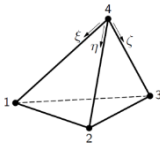
FE model (KT)



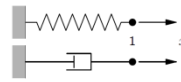
FE model (IC)



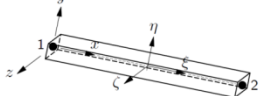
LE12L:  
Tetrahedron,  
3sides,  
4nodes  
(solid)



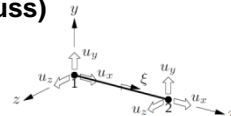
SP1TR: Translation,  
1node (spring)



L13BE: Straight, 2nodes,  
with shear (beam)

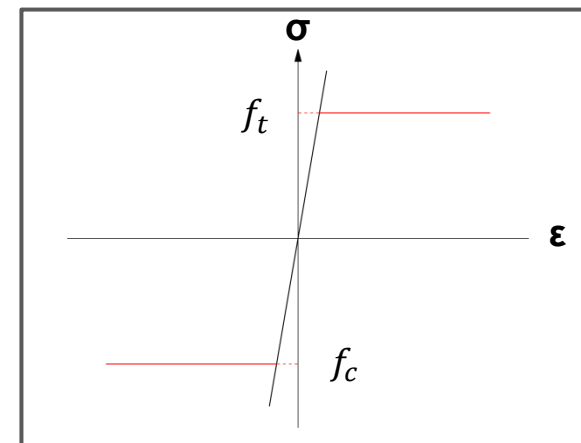
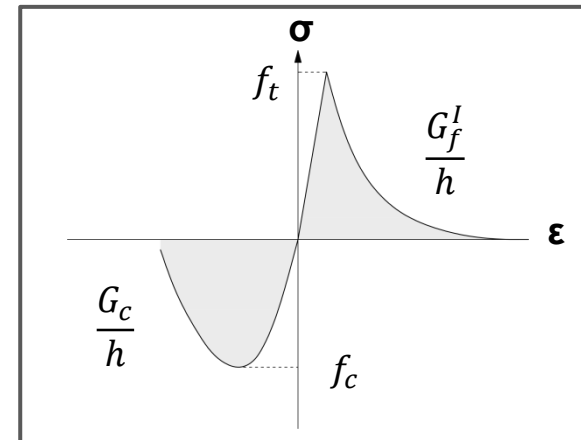


L6TRU: Straight, 2nodes  
(truss)



## Material properties and mechanical characterization

- ❑ Use of **building standards codes** (e.g. EC6, NTC 2008, RNE 2006) and results from **tests**
- ❑ **Masonry**
  - Nonlinear behaviour (Total Strain Rotating Crack Model)
- ❑ **Timber**
  - Isotropic homogeneous and linear elastic behaviour
  - Von Mises criterion

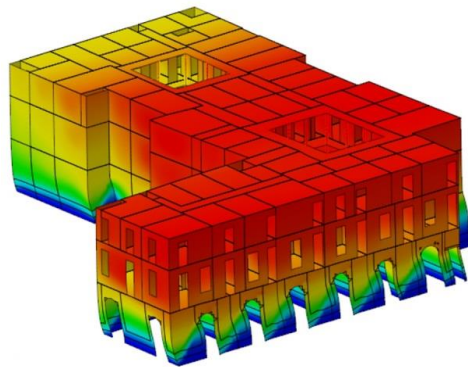
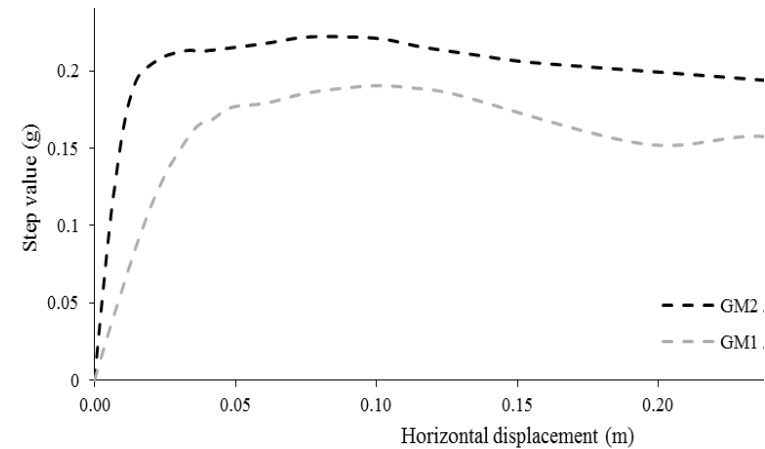
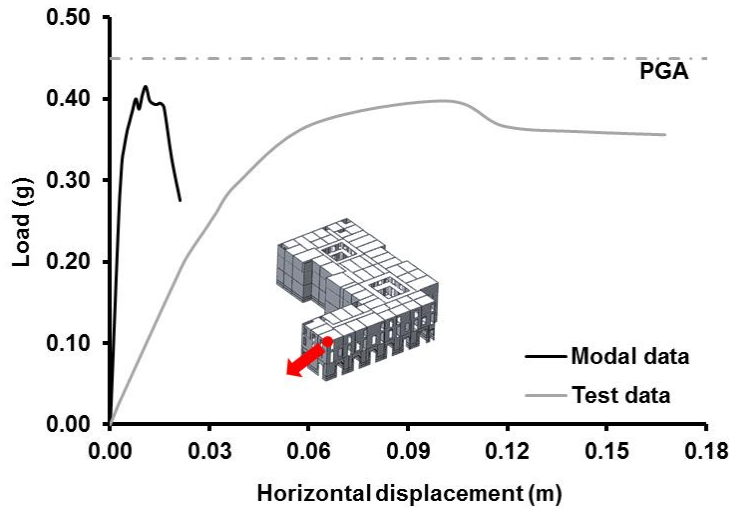


## Short note on material properties (I)

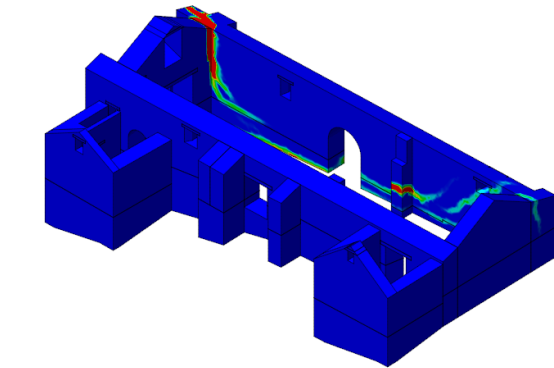
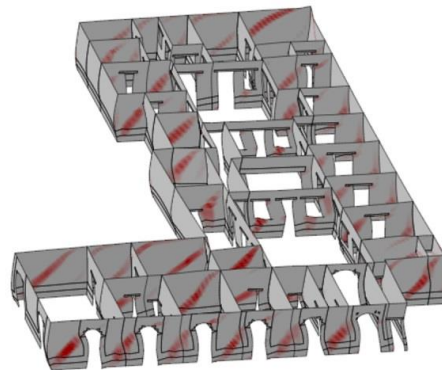
- ❑ The safety structures of historical masonry structures is usually geometry controlled, meaning that material properties tend to have a moderated influence on force based assessment
  
- ❑ Elastic properties were surprisingly complex to estimate and this affects to a great extent deformation response
  - ❑ Adobe masonry:
    - Tests in literature.  $E = 30$  to  $200$  MPa
    - Tests with actual materials.  $E = 70$  to  $100$  MPa
    - Sonic testing & dynamic identification.  $E = 250$  to  $300$  MPa
  - ❑ Quincha walls:
    - Tests with actual materials.  $E = 50$  MPa (no plaster)
    - Dynamic identification.  $E = 3000$ - $4000$  MPa (different levels)



## Short note on material properties (II)



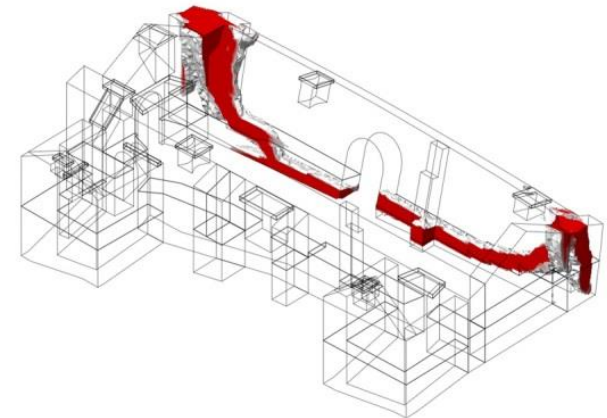
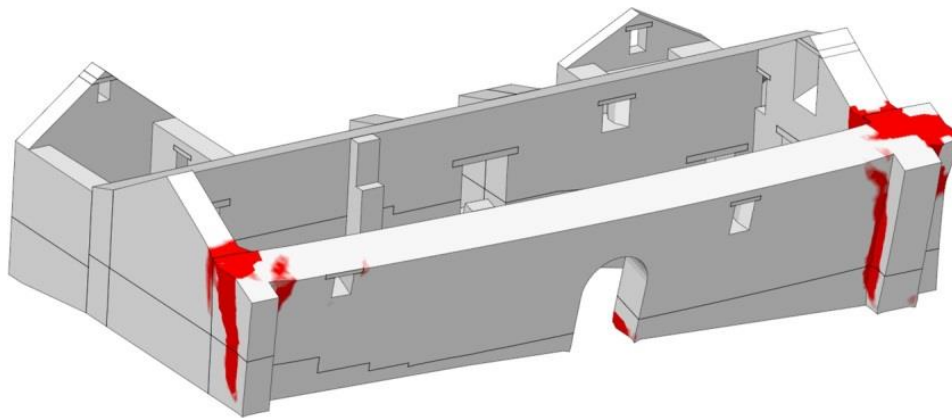
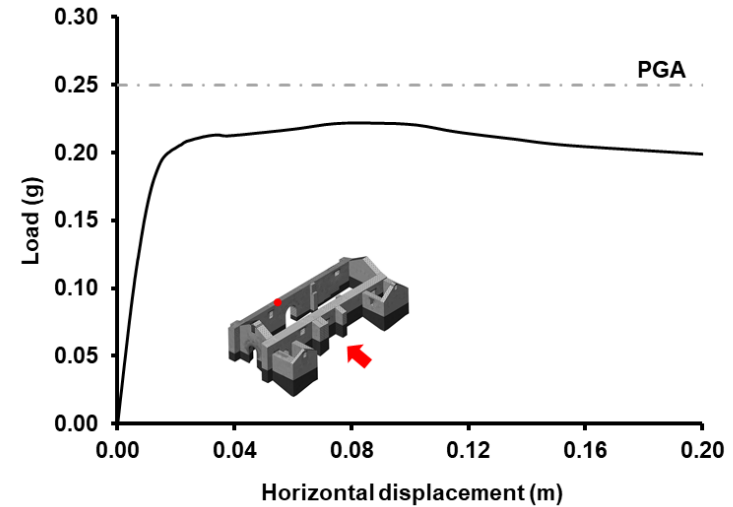
Hotel El Comercio (5% difference)



Church Kuño Tambo (15% difference)

## Pushover analysis (KT)

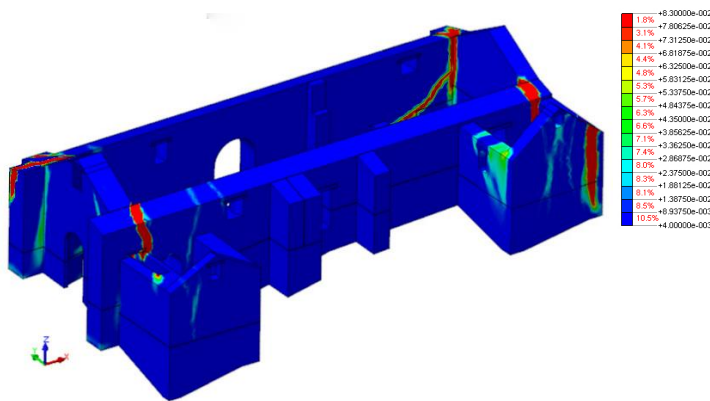
- ❑ Minimum seismic capacity of **0.20g**, lower than the design PGA (0.25g)
- ❑ Out-of-plane overturning of the **southern lateral wall**



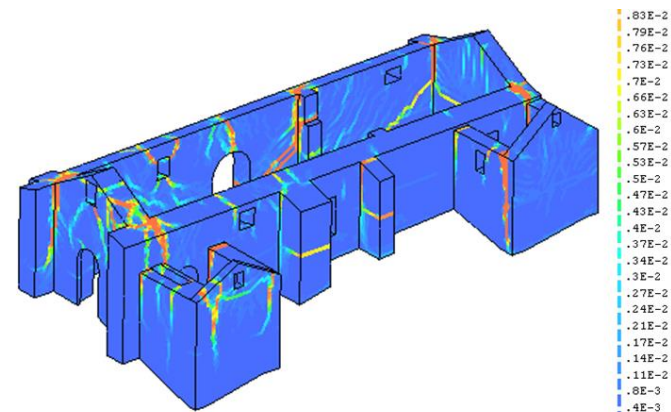
## Validation of the numerical model (KT)



Existing damage



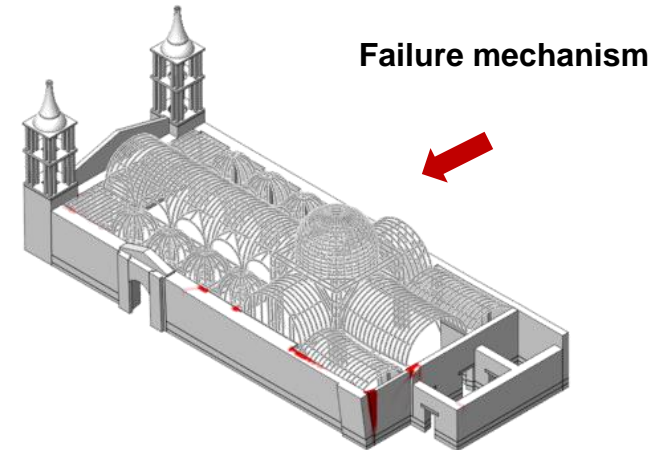
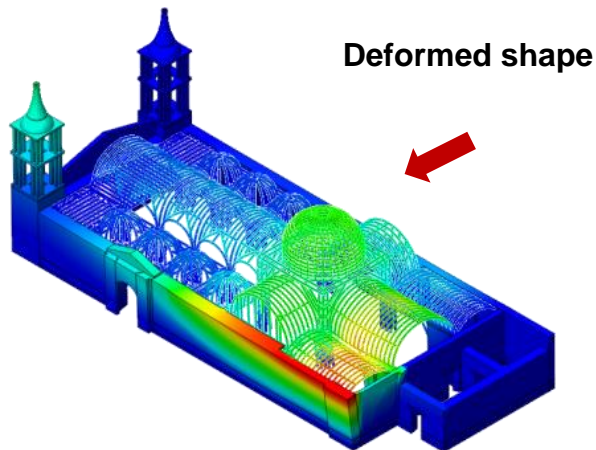
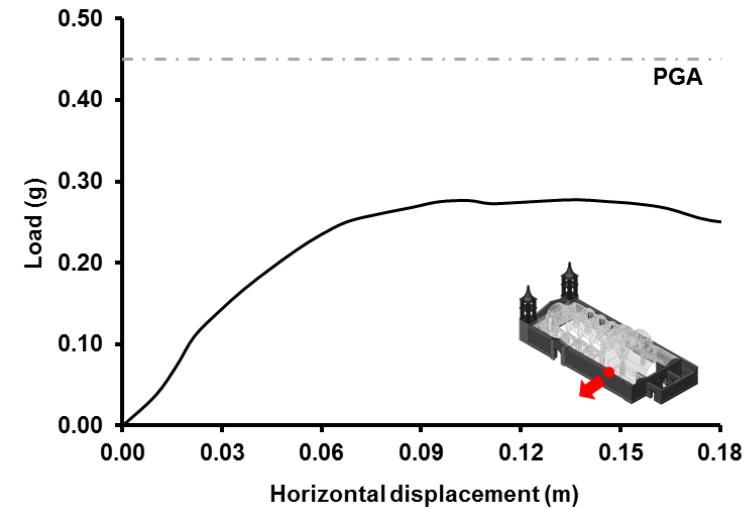
Pushover analysis - Max principal strains superposition



Time History analysis - Max principal strains

## Pushover analysis (IC)

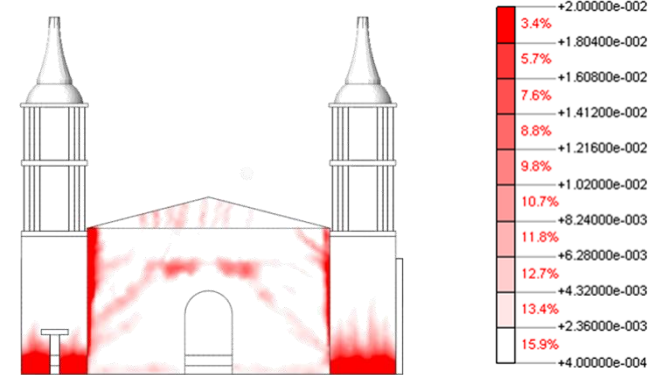
- ❑ Minimum seismic capacity of **0.28g**, much lower than the design PGA (0.45g)
- ❑ Out-of-plane mechanism of the **northern lateral wall**



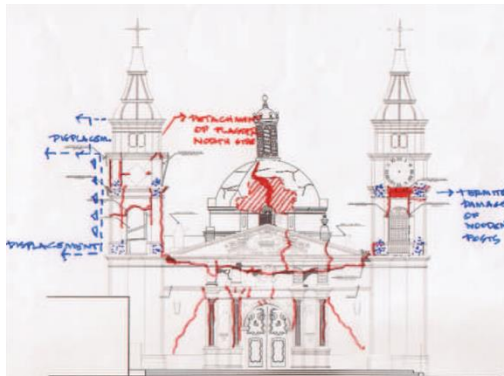
# Validation of the numerical model (IC)



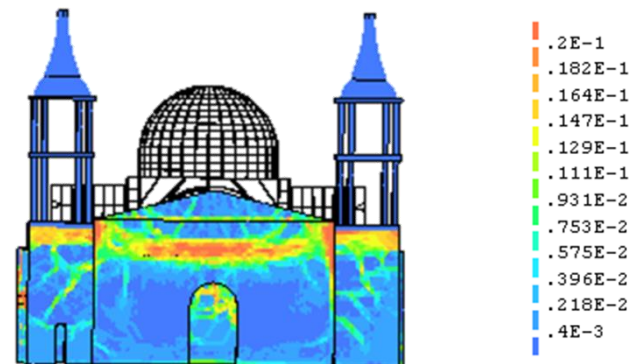
Existing Damage



Pushover Analysis - Max Principal Strains



In-situ damage survey (Cancino et al, 2015)



Time History Analysis - Max Principal Strains

**Strengthening**

**isise**



**Universidade do Minho**

## Philosophy and guidelines

- ❑ **Conservation principles** (ICOMOS, 2003)
  - Minimal intervention, safety, authenticity, reversibility, durability, material compatibility
  - **Guidelines** and **recommendations** in seismic building codes and standards for new earthen buildings

|             | Technical Norm  | Description  |
|-------------|---|--|
| PERU        | Norma E.030 (2016)                                    | Design of earthquake resistance of buildings                                   |
|             | RNE E.10 (2006)                                       | Design of timber elements for structural use                                   |
|             | Junta del Acuerdo de Cartagena<br>PADT- REPORT (2000) | Design manual for timber of the Andean group                                   |
|             | Norma E.080 (2017)                                    | Guidelines for design of reinforced adobe structures                           |
| NEPAL       | NBC 204 (1994)  | Guidelines for earthquake resistant building construction in earthen buildings |
| INDIA       | IS.13827 (1993)                                       | Guidelines for improving earthquake resistance of earthen buildings            |
| NEW ZEALAND | NZS 4297:1998   | Engineering design of earth buildings  |
|             | NZS 4298:1998   | Materials and workmanship for earth buildings                                  |

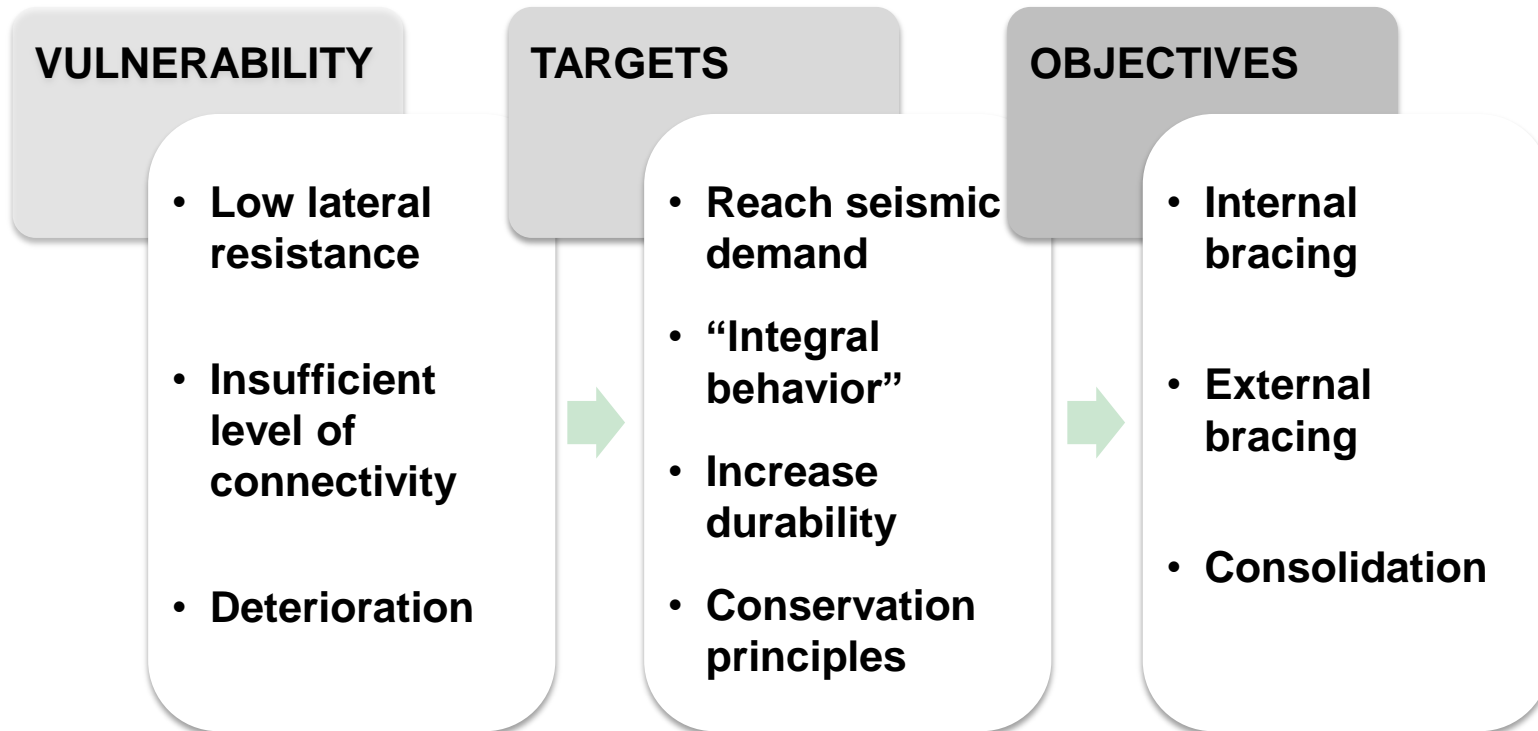
# Philosophy and guidelines

| Ica Cathedral           |                         | Engineering principles |                  |                   |               |
|-------------------------|-------------------------|------------------------|------------------|-------------------|---------------|
|                         |                         | Safety (470)           | Durability (430) | Feasibility (410) | Economy (400) |
| Conservation principles | Min. intervention (150) | 30 / 70                | 30 / 70          | 40 / 60           | 50 / 50       |
|                         | Reversibility (160)     | 40 / 60                | 40 / 60          | 40 / 60           | 40 / 60       |
|                         | Authenticity (260)      | 50 / 50                | 70 / 30          | 70 / 30           | 70 / 30       |
|                         | Arch. Config. (260)     | 50 / 50                | 70 / 30          | 70 / 30           | 70 / 30       |
|                         | Orig. material (130)    | 30 / 70                | 30 / 70          | 30 / 70           | 40 / 60       |
|                         | Trad. Techniques (160)  | 40 / 60                | 40 / 60          | 40 / 60           | 40 / 60       |
|                         | New/Orig. (170)         | 40 / 60                | 40 / 60          | 50 / 50           | 40 / 60       |
|                         | Compatibility (200)     | 50 / 50                | 50 / 50          | 50 / 50           | 50 / 50       |

| Church of Kuño Tambo    |                         | Engineering principles |                  |                   |               |
|-------------------------|-------------------------|------------------------|------------------|-------------------|---------------|
|                         |                         | Safety (430)           | Durability (340) | Feasibility (240) | Economy (290) |
| Conservation principles | Min. intervention (220) | 40 / 60                | 40 / 60          | 70 / 30           | 70 / 30       |
|                         | Reversibility (220)     | 40 / 60                | 50 / 50          | 70 / 30           | 60 / 40       |
|                         | Authenticity (260)      | 50 / 50                | 70 / 30          | 70 / 30           | 70 / 30       |
|                         | Arch. Config. (260)     | 50 / 50                | 70 / 30          | 70 / 30           | 70 / 30       |
|                         | Orig. material (280)    | 70 / 30                | 70 / 30          | 70 / 30           | 70 / 30       |
|                         | Trad. Techniques (200)  | 30 / 70                | 50 / 50          | 70 / 30           | 50 / 50       |
|                         | New/Orig. (210)         | 40 / 60                | 50 / 50          | 70 / 30           | 50 / 50       |
|                         | Compatibility (250)     | 50 / 50                | 60 / 40          | 40 / 60           | 70 / 30       |



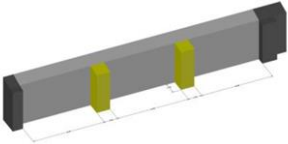
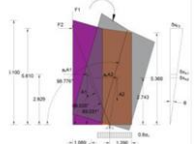
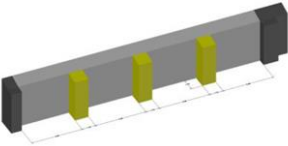
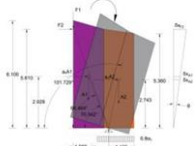
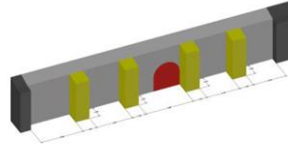
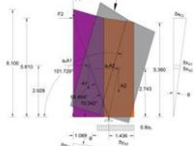
# Methodology

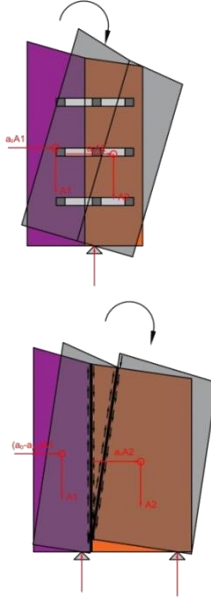


## Strengthening techniques

### □ Buttresses

- To address out-of-plane mechanisms of **large span walls**
- Design with **simple analysis tools** (Limit Analysis)
- **Proper connection** between the existing earthen walls

|                             | Design proposal   | Kinematic mechanism   | DLS | ULS | Displacement control | $a_0^*$ |
|-----------------------------|---|---|-----|-----|----------------------|---------|
| 2 Buttresses                |    |    | ✓   | ✓   | ✓                    | 0.28g   |
| 3 Buttresses                |    |    | ✓   | ✓   | ✓                    | 0.32g   |
| 4 Buttresses in full height |  |  | ✓   | ✓   | ✓                    | 0.37g   |



**Design of buttresses (KT)**

## Strengthening techniques

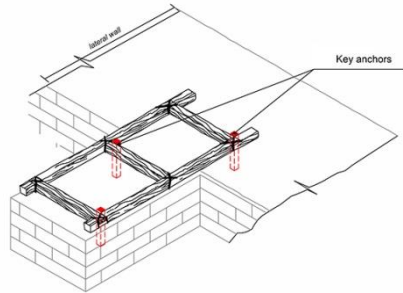
- ❑ **Bracing elements** (*corner keys, horizontal keys, bond beams and anchored tie beams*)
  - To improve the connection between **walls, wall-to-floor** and **wall-to-roof connections**
  - Located at **various levels**, involving mostly the upper parts
  - **Confinement in masonry** and **friction** or **shear action**



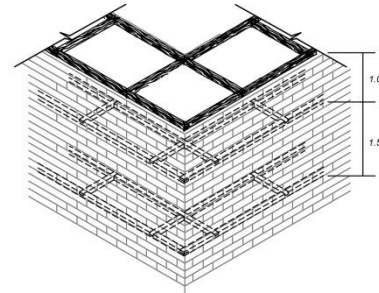
Experimental results on pull-out tests from PUCP

# Strengthening techniques

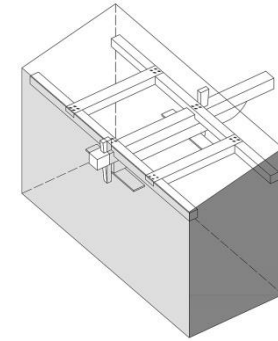
## □ Bracing elements (KT)



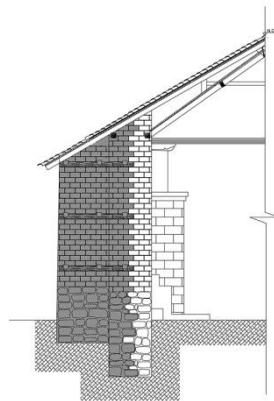
Horizontal timber key between buttress and adjoining wall. Vertical key anchors to enhance connectivity



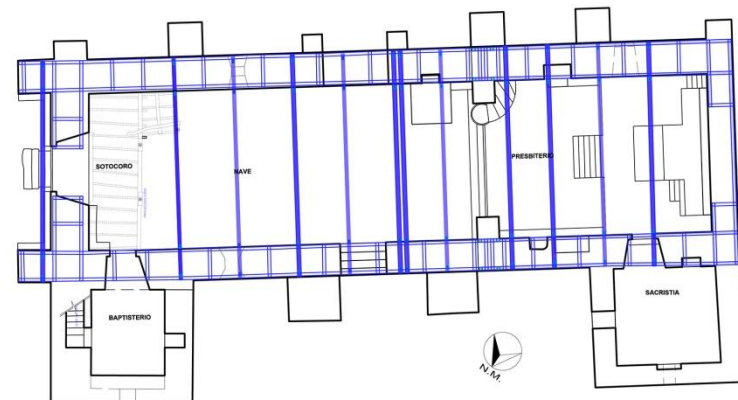
Timber embedded corner keys in elevation. Continuous bond beam at top



Bond beam, tie beam and vertical timber anchors

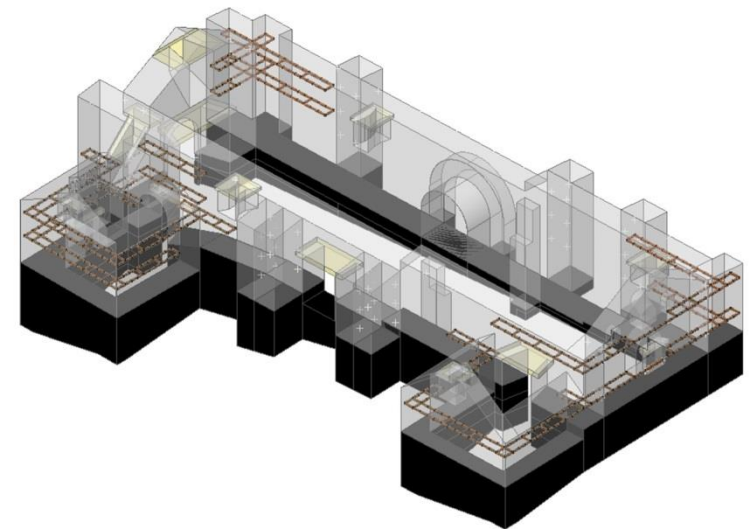
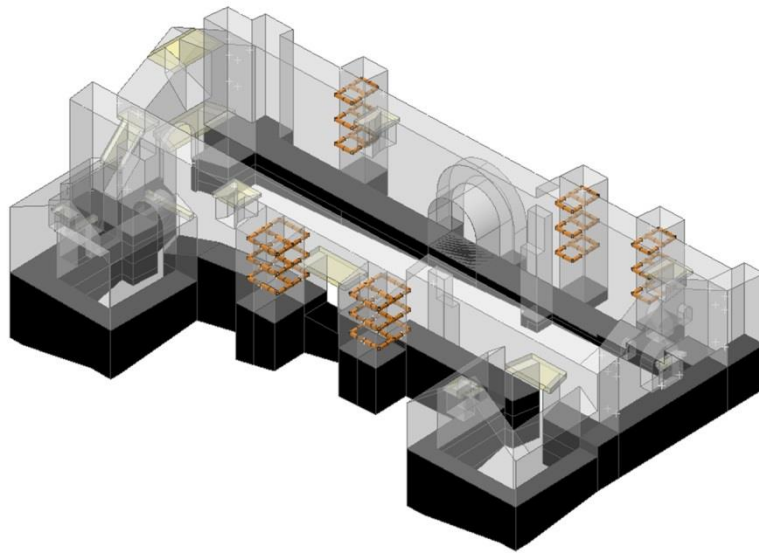
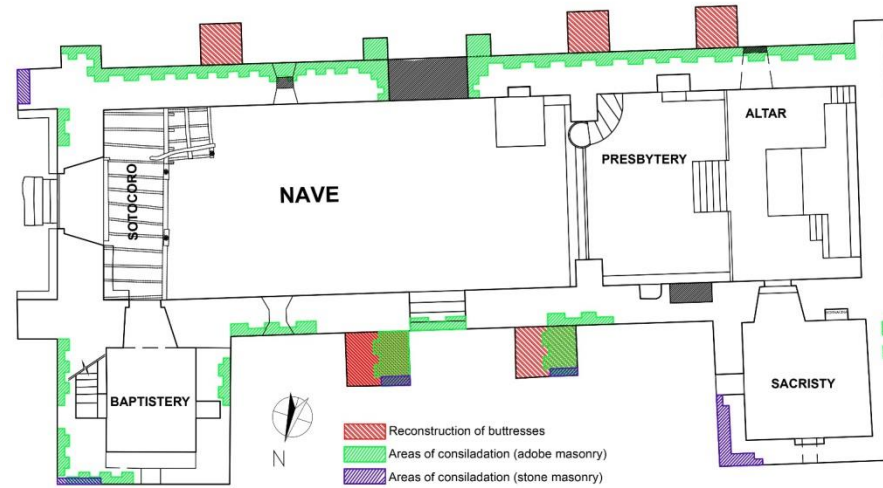


New buttress with horizontal timber keys and interlocking, and geo-mesh, lower part of stabilized adobe (replaced by brick masonry during execution)

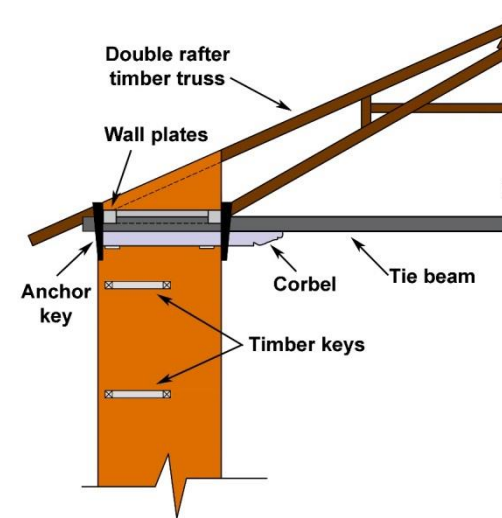
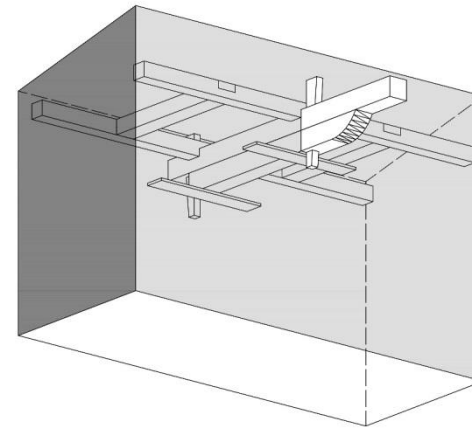
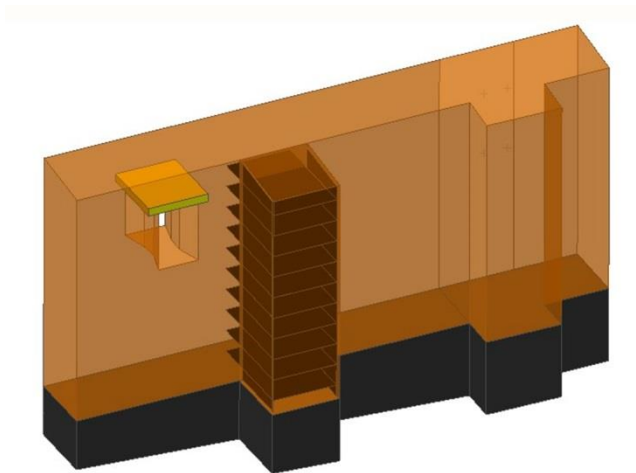


Bond-beam at top eaves. Configuration with two longitudinal timber beams and transversal timber blockers. Connection with tie beams

# Kuño Tambo (I)

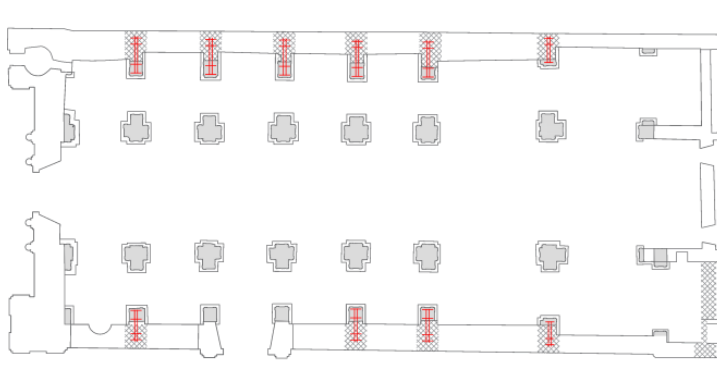


# Kuño Tambo (II)

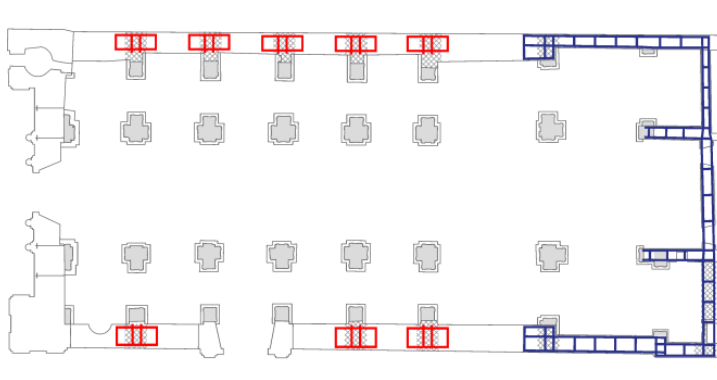


# Strengthening techniques

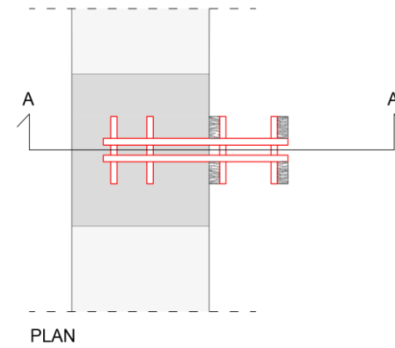
## □ Bracing elements (IC)



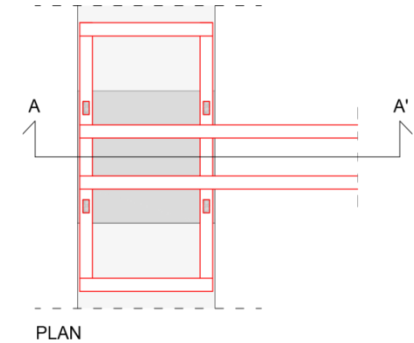
Timber anchoring system at the lower levels



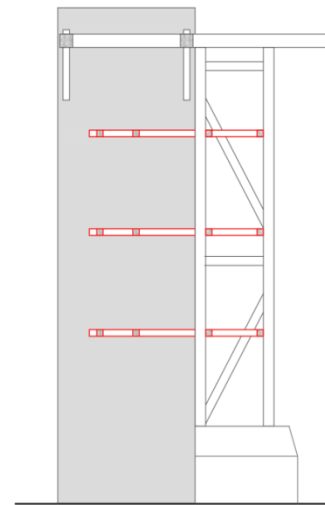
Timber anchoring system at the upper level



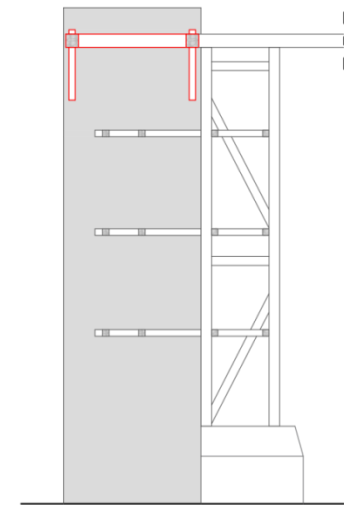
PLAN



PLAN



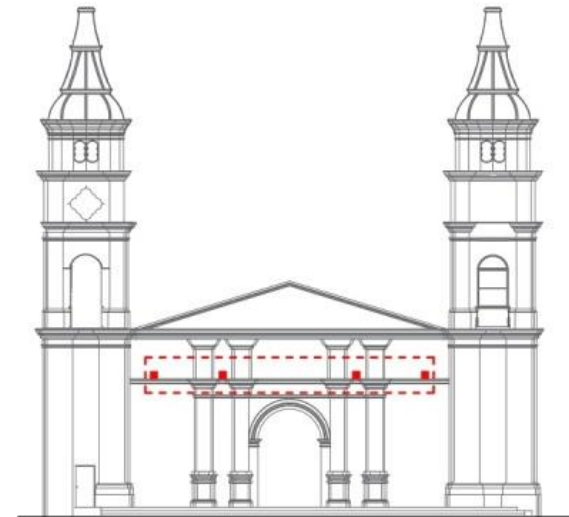
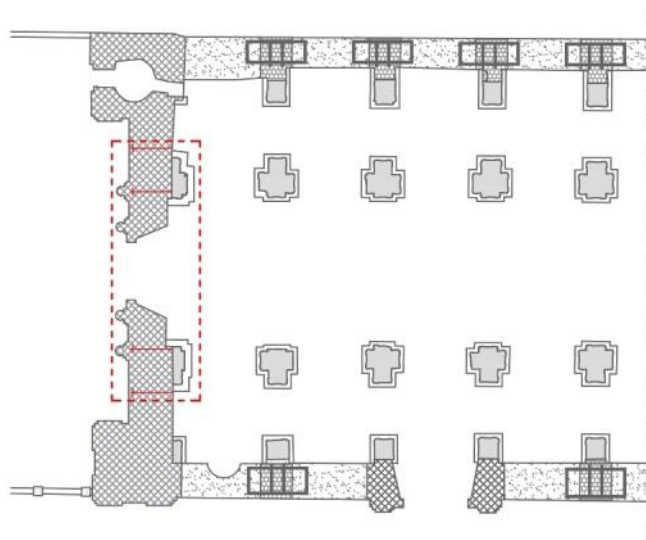
SECTION A - A'



SECTION A - A'

## Strengthening techniques

### ❑ Bracing elements (IC)

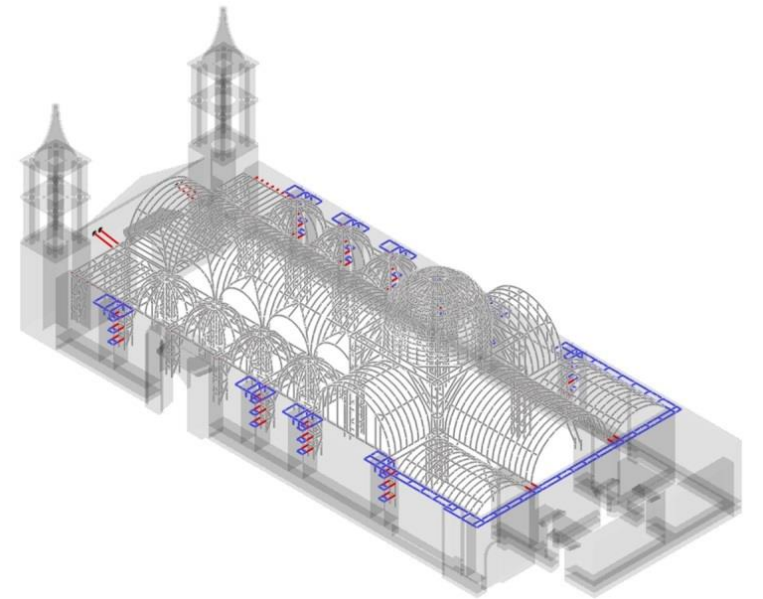
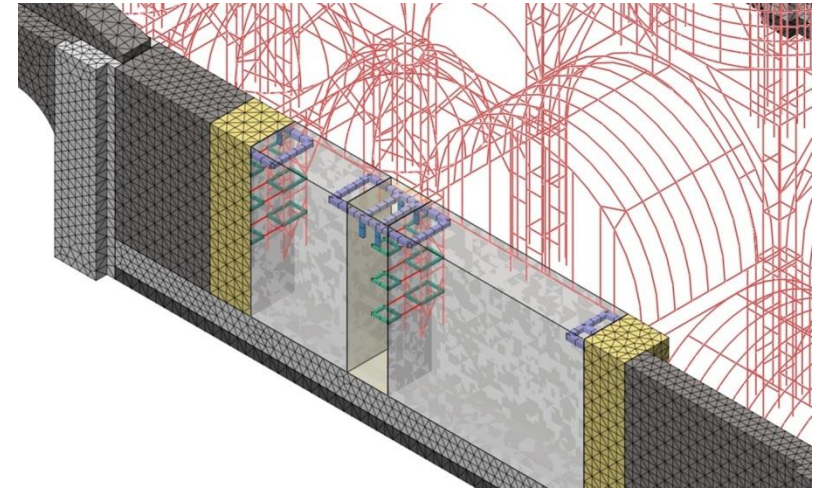
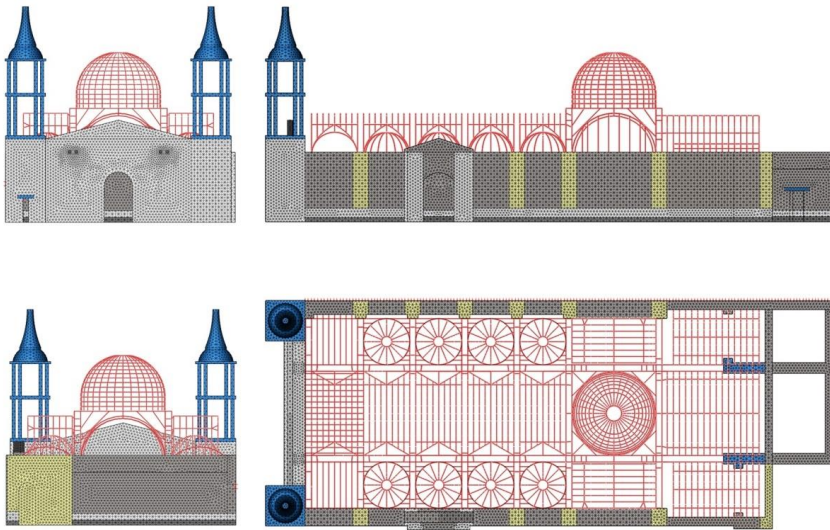


Steel anchoring system at the main façade



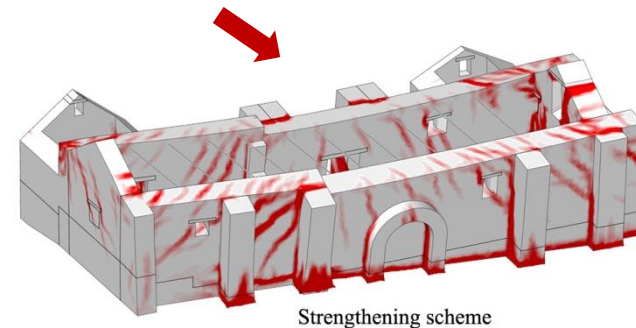
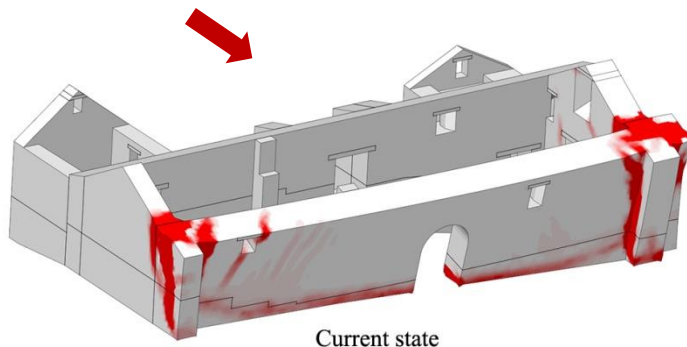
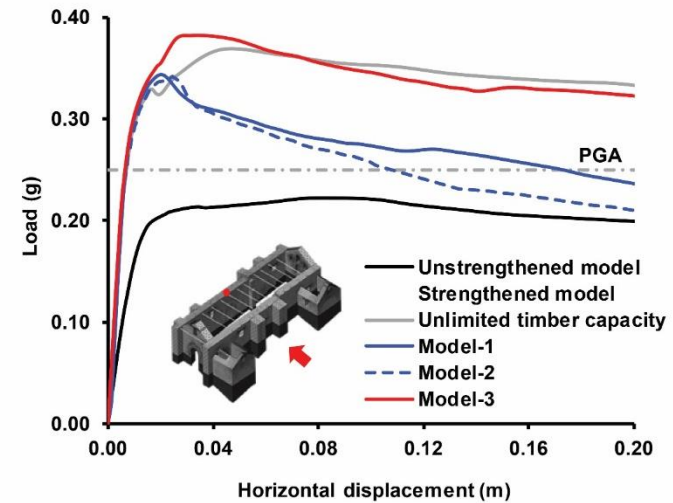


# Ica Cathedral



## Pushover analysis (KT)

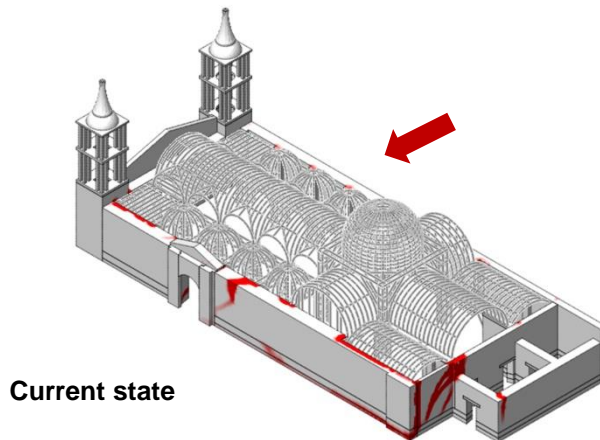
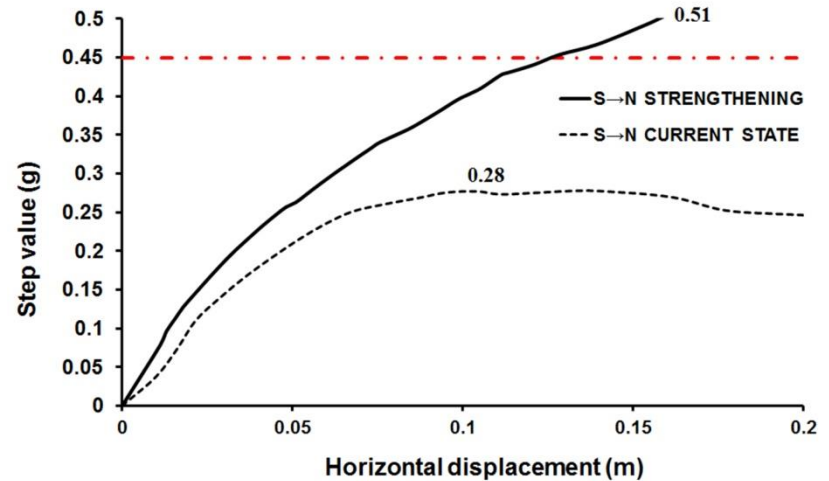
- ❑ Seismic capacity of **0.34g**, higher than the design PGA
- ❑ Out-of-plane bending mechanism, with more masonry involved
- ❑ Damage widely spread, with smaller crack width



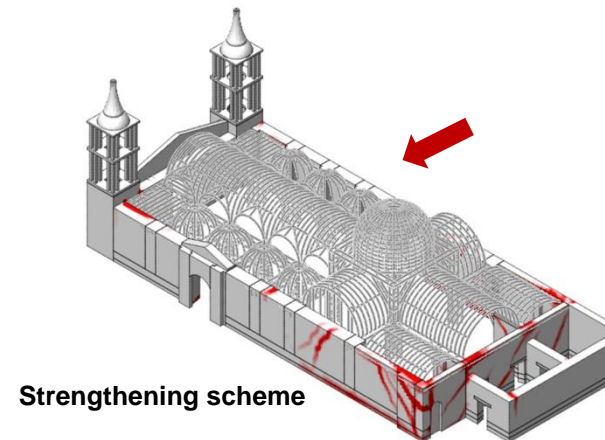
Failure mechanism in terms of tensile strains

## Pushover analysis (IC)

- ❑ Seismic capacity higher than the design PGA (**0.45g**)
- ❑ Out-of-plane bending mechanism, activating both the longitudinal walls
- ❑ Damage more distributed in the north-west corner



Current state

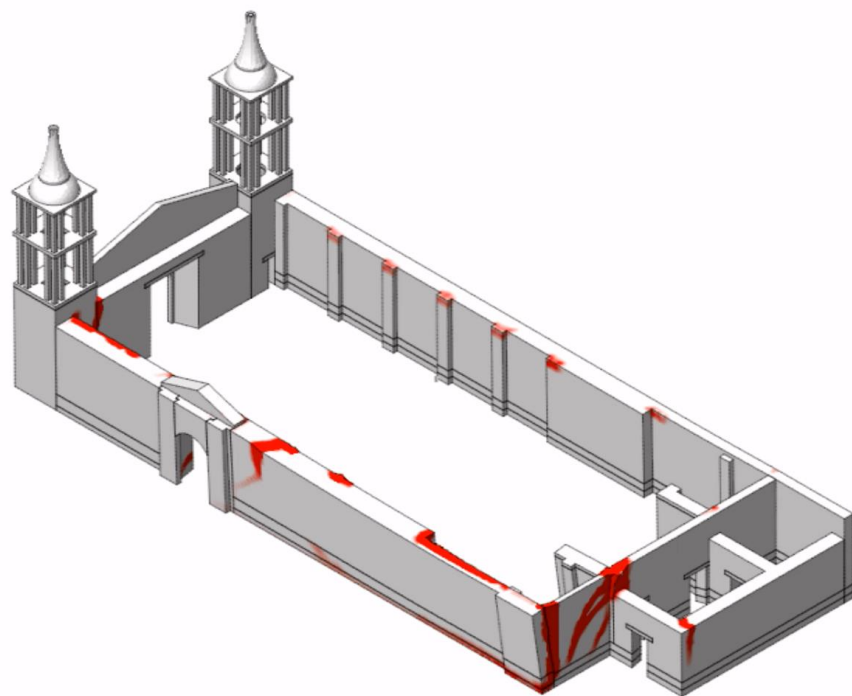


Strengthening scheme

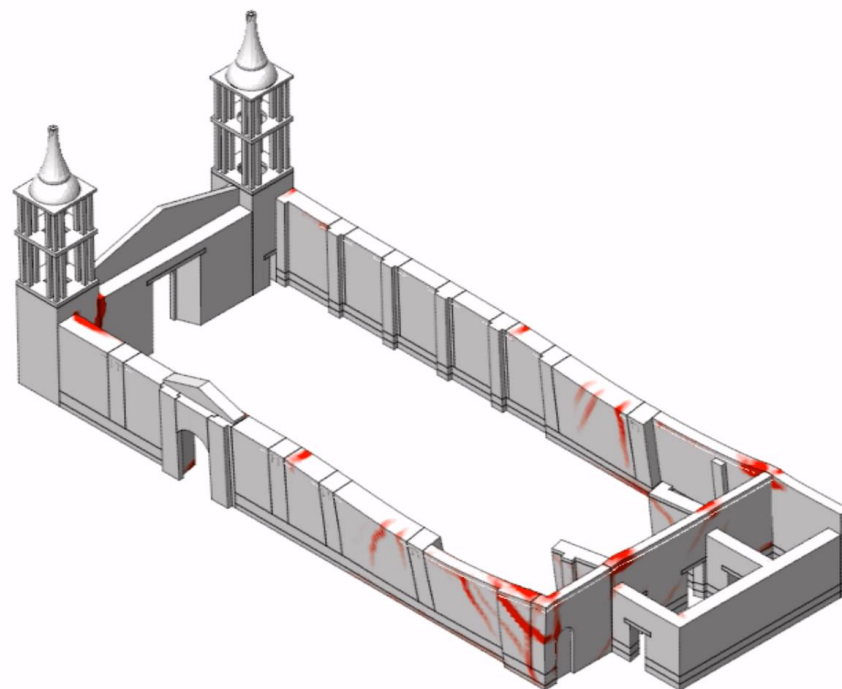
Failure mechanism in terms of tensile strains

## Pushover analysis (IC)

**Non-strengthened**



**Strengthened**



# Conclusions

isise



## Conclusions

- ❑ Out-of-plane failure of masonry is a critical issue for historic structures. Remains a challenge under dynamics but our predictions seem conservative
- ❑ Adequate structural analysis methods are available for existing cultural heritage buildings, allowing reasonable predictions of safety and providing assistance in designing strengthening measures
- ❑ Based on recommendations from national building codes, conservation principles and local practices, innovative traditional strengthening techniques can improve the integrity of earthen and masonry structures
- ❑ The results obtained for KT and IC after strengthening show:
  - An improved global seismic behaviour of the structures
  - Compliance with seismic local demand

## Conclusions

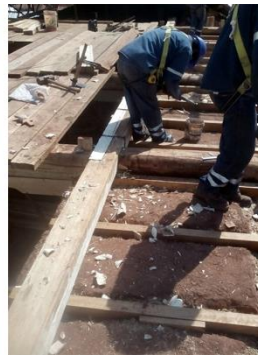




## Conclusions



# Conclusions



## Conclusions



# Technologies for Seismic Retrofitting and Strengthening of Earthen and Masonry Structures: Assessment and Application

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